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**PROPULSION SYSTEM FLOW STABILITY PROGRAM  
(DYNAMIC)**

**PHASE I FINAL TECHNICAL REPORT,  
PART XX - COMPUTER PROGRAMS FOR THE ROOT LOCUS ANALYSIS  
OF LINEARIZED TURBOJET AND TURBOFAN CONTROL SYSTEMS.**

E. L. Lum  
AUTONETICS DIVISION OF NORTH AMERICAN ROCKWELL CORPORATION

TECHNICAL REPORT AFAPL-TR-68-142, PART XX

F33615-67-C-1848

December 1968

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Air Force Aero Propulsion Laboratory  
Air Force Systems Command  
Wright-Patterson Air Force Base, Ohio

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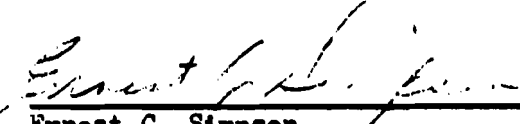
## FOREWORD

This report describes work accomplished in Phase I of the two-phase program, "Propulsion System Flow Stability Program (Dynamic)" conducted under USAF Contract F33615-67-C-1848. The work was accomplished in the period from 20 June 1967 to 30 September 1968 by the Los Angeles Division of North American Rockwell Corporation, the prime Contractor, and the Subcontractors, the Allison Division of General Motors Corporation (supported by Northern Research and Engineering Corporation), the Autonetics Division of North American Rockwell Corporation (supported by the Aeronautical Division of Honeywell, Incorporated), and the Pratt & Whitney Aircraft Division of United Aircraft Corporation.

The program was sponsored by the Air Force Aero Propulsion Laboratory, Wright-Patterson Air Force Base, Ohio. Mr. H. J. Gratz, APTA, Turbine Engine Division, was the Project Engineer.

This volume is Part XX of twenty parts and was prepared by the Autonetics Division of North American Rockwell Corporation.

Publication of this report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

  
Ernest C. Simpson  
Chief, Turbine Engine Division

## ABSTRACT

This part describes computer programs developed to handle the computational tasks for the linear stability analysis of propulsion controls by root locus techniques. The descriptions, flowcharts, and Fortran program listings of two main programs TJET and TFAN developed for the analysis of turbojet and turbofan engine control systems are presented. Also presented are the descriptions of three subroutines specially developed to facilitate data handling for this study. Examples are given to illustrate the application of computer programs TJET and TFAN.

TJET and TFAN have been valuable in the linear analysis of the propulsion system. However, it is recommended that these computer programs be expanded to include the capability of analyzing coupled control loops and to include a limited transient analysis.



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## I. INTRODUCTION

Computer programs TJET and TFAN were developed to aid in the linear analysis of the turbojet and turbofan engine control systems, respectively, under the Propulsion System Flow Stability Program. These computer programs compute the closed loop characteristic of the engine control systems for stability analysis by root locus techniques. A brief introduction and discussion of root locus techniques follows.

The Laplace transform representation of a simple control loop is shown in Figure 1, where  $K_c$  is the control gain which may be varied and  $G_p$  is the  $s$ -plane transfer function of the open loop system, or plant. The numerator,  $N_p$ , and denominator,  $D_p$ , of the  $s$ -plane transfer function,  $G_p$ , are both polynomials in  $s$ . The roots of  $N_p$  are called the open loop zeros and the roots of  $D_p$  are called the open loop poles.

The transfer function of the closed loop system of Figure 1 is

$$\frac{C}{R}(s) = \frac{K_c G_p}{1 + K_c G_p} = \frac{K_c N_p}{D_p + K_c N_p} \quad (1)$$

The denominator of Equation (1) characterizes the closed loop behavior of the system and is thus called the closed loop characteristic,  $D_{CL}$ , or

$$D_{CL} = D_p + K_c N_p \quad (2)$$

By root locus techniques, the roots of  $D_{CL}$ , or closed loop poles, are plotted in the complex  $s$ -plane as a function of varying  $K_c$ , from which the stability and frequency response characteristics of the closed loop system may be observed. The operations required to obtain the root locus of  $D_{CL}$  is (a) perform the polynomial addition indicated by the right hand side of Equation (2), and (b) factor the resulting polynomial to obtain the roots.

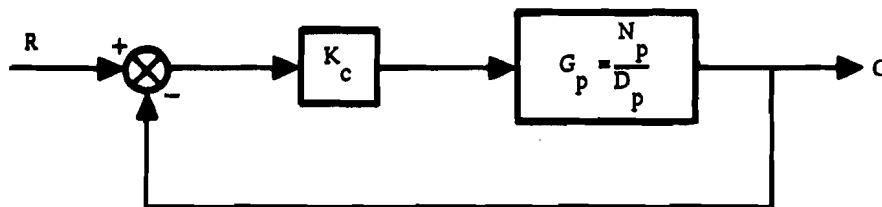


Figure 1. Simple Control Loop Block Diagram



For the general case, a complex control system may have many control loops with many control gains to be determined. However, any linear control system can be reduced to the form of the simple case of Figure 1, with  $G_p$  representing a system transfer function with control loops already closed. Actually, computing  $G_p$  for coupled control systems is a rather complicated process, especially when all actuators and sensor dynamics are incorporated. But once  $G_p$  is determined for a particular control loop, all that is required to compute the closed loop characteristic for that loop is the simple procedure of Equation (2). In this fashion, one may close control loops around other control loops, or may close loops simultaneously, which is what TJET and TFAN were designed for.

The present versions of TJET and TFAN as presented in this section are useful only for the analysis of a single loop closure because the necessary cross-coupling terms discussed in Part XIX, were not included in the equations used in programming TJET and TFAN. This omission was made because the available transfer function data did not include the necessary cross-coupling terms anyway. Hence, although TJET and TFAN are set up for sequential loop closures, the results for varying more than one control gain will not be valid unless the control loops involved are not strongly coupled, which is not the case here. The present versions of TJET and TFAN do, however, provide the framework for coupled multiloop control analysis of the respective engines, and with a few modifications, the required cross-coupling terms can be included in TJET and TFAN, if and when such an analysis is desirable.

Main programs TJET and TFAN and all non-library subprograms required are programmed in Fortran IV, level H for the IBM 360. Compiler option (OPT = 2) was used to optimize the execution speed and reduce the size of the object deck. Descriptions, flowcharts and listings of the Fortran programs developed for the Propulsion System Flow Stability Program linear control analysis follow.

## II. DESCRIPTION OF MAIN PROGRAM TJET

### BLOCK DIAGRAM AND NOMENCLATURE

The two control systems for the turbojet engine under study are (1) the turbojet rotor speed control loop, or Speed Control, in short, and (2) the turbojet turbine discharge temperature control, or the Temperature Control, in short. The block diagrams for the subject control systems are shown in Figure 2. The nomenclature used for this figure and for the control equations are defined in Table I.  $K_{WNA}$ ,  $K_{AT}$ ,  $K_{NT}$ ,  $K_{TN}$ ,  $K_{N2A}$  and  $K_{T6A}$  are the control gains to be determined.

Program TJET allows for the variation of the control gains  $K_{WNA}$ ,  $K_{AT}$ ,  $K_{NT}$  and  $K_{TN}$ , individually, or in sequence. The integrator gains  $K_{N2A}$  and  $K_{T6A}$  are preselected. Individual control loops are investigated by setting the control gains in the other control loops to zero. For example, to investigate the Speed Control loop, one sets  $K_{AT} = K_{TN} = 0$ .

To illustrate how TJET closed control loops sequentially, the following notation is used,

$$D_{CL} = F(K_c, G_p) \quad (3)$$

where  $F$  denotes the polynomial addition process indicated by the right hand side of Equation (2). Then, if it is desired to vary  $K_{WNA}$ ,  $K_{AT}$ ,  $K_{NT}$  and  $K_{TN}$  sequentially, TJET will perform the following operation

$$D_{CL} = F_4(K_{WNA}, F_3(K_{AT}, F_2(K_{NT}, F_1(K_{TN}, G_p)))) \quad (4)$$

where  $F_i$  ( $i = 1, 2, 3, 4$ ) indicates the operation defined by Equation (3) with  $F_1$  evaluated first,  $F_2$  next, etc. In the programming of TJET, this is implemented by nested DO loops (see flowchart and listing of TJET). If one or more of the gains  $K_{WNA}$ ,  $K_{AT}$ ,  $K_{NT}$  or  $K_{TN}$  is set to zero, then the operation indicated by Equation (3) is bypassed for that control gain by logic statements in the program, enabling the investigation of individual control loops separately.

### EQUATIONS FOR LINEAR ANALYSIS OF TURBOJET ENGINE

The closed loop characteristic (DF) of the turbojet engine control, without coupling between control loops, is (using the same notation as defined for the arrays of TJET)

$$(DF) = (CA) + \left[ K_{WNA} (CB) + (CC) \right] + K_{AT}(CD) \\ + K_{NT}(CE) + K_{TN}(CF)$$

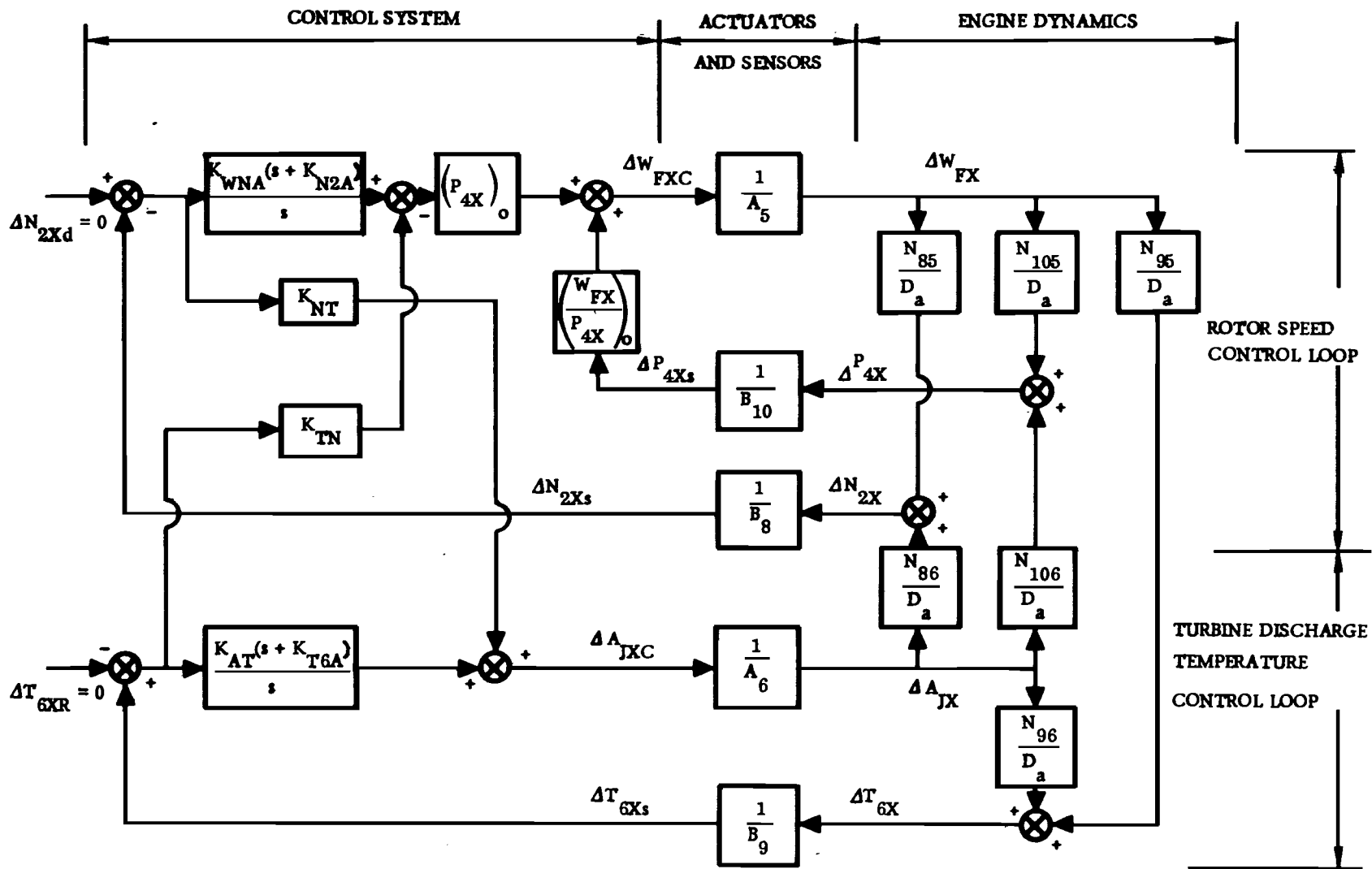


Figure 2. Turbojet Engine Linear Control System Block Diagram

Table I. Nomenclature for Analysis of Turbojet Engine Control

a) Sensed and Actuated Variables

Actuated Variables,  $x_j$

$x_5 = W_{FX}$  Turbojet Main Combustor Fuel Flow (lb/hr)

$x_6 = A_{JX}$  Turbojet Exhaust Nozzle Area (ft<sup>2</sup>)

Sensed Variables,  $y_i$

$y_8 = N_{2X}$  Turbojet Rotor Mechanical Speed (RPM)

$y_9 = T_{6X}$  Turbojet Turbine Discharge Temperature (°R)

$y_{10} = P_{4X}$  Turbojet Compressor Discharge Pressure (psia)

b) Actuator and Sensor Definitions

$W_{FX}$  Actuator:  $1/A_5$

$A_{JX}$  Actuator:  $1/A_6$

$N_{2X}$  Sensor:  $1/B_8$

$T_{6X}$  Sensor:  $1/B_9$

$P_{4X}$  Sensor:  $1/B_{10}$

where  $A_j$  is the denominator of the actuator lag for  $x_j$ , and  $B_i$  is the denominator of the sensor lag for  $y_i$ .

c) Transfer Function Numerators

$N_{85} =$  Numerator of  $\partial N_{2X} / \partial W_{FX}$  transfer function

$N_{86} =$  Numerator of  $\partial N_{2X} / \partial A_{JX}$  transfer function

$N_{95} =$  Numerator of  $\partial T_{6X} / \partial W_{FX}$  transfer function

Table I. Concluded

$N_{96}$  = Numerator of  $\partial T_{6X} / \partial A_{JX}$  transfer function

$N_{105}$  = Numerator of  $\partial P_{4X} / \partial W_{FX}$  transfer function

In general,  $N_{ij}/D_a$  is the transfer function for the  $i$ -th dependent variable  $y_i$ , due to the  $j$ -th independent variable  $x_j$ .  $D_a$  is the open loop denominator of the turbojet engine dynamics.

where

1. Open-Loop Denominator ( $D_p$  of Equation 2)

$$(CA) = s A_5 A_6 B_8 B_9 B_{10} D_a$$

2. Numerators for speed loop closure

$$(CB) = (P_{4X})_0 A_6 B_9 B_{10} (s + K_{N2A}) N_{85}$$

$$(CC) = -s (W_{FX} / P_{4X})_0 A_6 B_8 B_9 N_{105}$$

3. Numerator for Temperature Loop Closure

$$(CD) = -A_5 B_8 B_{10} (s + K_{T6A}) N_{96}$$

4. Numerator for Variation in  $K_{NT}$

$$(CE) = s A_5 B_9 B_{10} N_{86}$$

5. Numerator for Variation in  $K_{TN}$

$$(CF) = s (P_{4X})_0 A_6 B_8 B_{10} N_{95}$$

Actually, TJET has logic statements which omit certain actuator poles,  $A_i$ , and sensor poles,  $B_j$ , from these equations if they are not affected by one of the loop closures. For example, if only the speed loop is closed, then  $A_6$  and  $B_9$  are not required in the computations.

#### FLOWCHART AND PROGRAM LISTING OF TJET

Table II defines the nomenclature used in the programming of computer program TJET. The flowchart for main program TJET is shown on Figure 3. The print-out statements are left out of the flowchart for clarity. The circled numbers in Figure 3 correspond to the statement numbers in the Fortran H program listing of TJET shown on Table III.

Table II. List of Subprograms and Variables Used for TJET

<b>a) <u>List of Subprograms Required for TJET</u></b>		
Non-library:		in Fortran H for IBM 360
(1) XPNP5		Expand a polynomial with 5 sets of first order lags
(2) GENP		Generate a polynomial from data of form given by P&WA
(3) XPNTAU		Expand a polynomial with a given set of first order lags
(4) PRTX <sup>1</sup>		Polynomial root extraction using Bairstow and Newton-Raphson iterations
(5) FLIP <sup>1</sup>		Reverse order of elements in an array
(6) POLYX <sup>2</sup>		Multiply two polynomials
(7) GPOL <sup>2</sup>		Multiply a polynomial by a constant
(8) POLADD <sup>2</sup>		Add two polynomials
(9) WRT <sup>2</sup>		Print roots of a polynomial
(a) WRTPOL <sup>2</sup>		Print coefficients of a polynomial
(10) PRIN <sup>2</sup>		Print non-zero elements of an array
Library:		for Fortran IV on IBM 360
(11) DECRD		Read variable length data in standard format
<b>b) <u>Arrays of Variables Used in TJET</u></b>		
DA	= D <sub>a</sub>	Open-loop denominator
N85	= N <sub>85</sub>	Numerator <sup>3</sup> of $\partial N_{2X} / \partial W_{FX}$ transfer function

<sup>1</sup>Developed by J. C. Long of NAR/Space Division

<sup>2</sup>Originally developed for ALODE's I and II, Automatic Linear Optimal Design and Evaluation Computer Programs

<sup>3</sup>Expressed either in terms of (1) coefficients of polynomial, or (2) first-order lags of polynomial, in which case FLG  $\neq$  0.

Table II. (Cont)

N86	= $N_{86}$	Numerator <sup>3</sup> of $\partial N_{2X}/\partial A_{JX}$ transfer function
N95	= $N_{95}$	Numerator <sup>3</sup> of $\partial T_{6X}/\partial W_{FX}$ transfer function
N96	= $N_{96}$	Numerator <sup>3</sup> of $\partial T_{6X}/\partial A_{JX}$ transfer function
N105	= $N_{105}$	Numerator <sup>3</sup> of $\partial P_{4X}/\partial W_{FX}$ transfer function
KWNA	= $K_{WNA}$	Control gains for rotor speed loop
KAT	= $K_{AT}$	Control gains for temperature loop
KNT	= $K_{NT}$	"Decoupling" gain
KTN	= $K_{TN}$	"Decoupling" gain
TA5	= $A_5$	Time constants of $W_{FX}$ actuator lag
TA6	= $A_6$	Time constants of $A_{JX}$ actuator lag
TB8	= $B_8$	Time constants of $N_{2X}$ sensor lag
TB9	= $B_9$	Time constants of $T_{6X}$ sensor lag
TB10	= $B_{10}$	Time constants of $P_{4X}$ sensor lag
F		Array for input of data using DECRD
TITLE		Title of run in alpha-numeric characters (up to 72 characters)
CA, CB, CC, CD, CE, CF		Arrays used for temporary storage of intermediate polynomials used in computations
DCL, DD, DE, DF		Arrays used for temporary storage of polynomials used to compute closed-loop characteristic polynomial
CAR, CAC (Complex)		Arrays used for temporary storage of the real and complex roots of a polynomial

<sup>3</sup> Expressed either in terms of (1) coefficients of polynomial, or (2) first-order lags of polynomial, in which case  $FLG \neq 0$ .



Table II. (Cont)

c) <u>Real *4 Variables</u>	
CPØ	1. if checkout print option desired
FLG	≠ 0. if data entered in form supplied by P&WA
G85	Steady-state gain for $\partial N_{2X}/\partial W_{FX}$ transfer function, only if FLG≠0
G86	Steady-state gain for $\partial N_{2X}/\partial A_{JX}$ transfer function, only if FLG≠0
G95	Steady-state gain for $\partial T_{6X}/\partial W_{FX}$ transfer function, only if FLG≠0
G96	Steady-state gain for $\partial T_{6X}/\partial A_{JX}$ transfer function, only if FLG≠0
G105	Steady-state gain for $\partial P_{4X}/\partial W_{FX}$ transfer function, only if FLG≠0
KN2A = $K_{N2A}$	Integrator gain for speed loop
KT6A = $K_{T6A}$	Integrator gain for temperature loop
P4A = $(P_{4X})_0$	Initial steady-state value of $P_{4X}$
WFA = $(W_{FX})_0$	Initial steady-state value of $W_{FX}$
SF	Scale factor for roots (used as a dummy argument when calling subroutine PRTX)
d) <u>Integer *4 Variables</u>	
NDA	Degree of open loop denominator polynomial (array DA)
NN85	Degree of numerator for $\partial N_{2X}/\partial W_{FX}$ transfer function
NN86	Degree of numerator for $\partial N_{2X}/\partial A_{JX}$ transfer function
NN95	Degree of numerator for $\partial T_{6X}/\partial W_{FX}$ transfer function
NN96	Degree of numerator for $\partial T_{6X}/\partial A_{JX}$ transfer function
NN105	Degree of numerator for $\partial P_{4X}/\partial W_{FX}$ transfer function

Table II. (Cont)

NTA5	Number of first-order lags for $W_{FX}$ actuator
NTA6	Number of first-order lags for $A_{JX}$ actuator
NTB8	Number of first-order lags for $N_{2X}$ sensor
NTB9	Number of first-order lags for $T_{6X}$ sensor
NTB10	Number of first-order lags for $P_{4X}$ sensor
NWNA	Number of $K_{WNA}$ gains for which root locus is computed
NAT	Number of $K_{AT}$ gains for which root locus is computed
NNT	Number of $K_{NT}$ gains for which root locus is computed
NTN	Number of $K_{TN}$ gains for which root locus is computed

The following integers are used for indexing only: I, NA, NB, NC, ND.  
 The following integers are used to indicate size of arrays in computations:  
 (Example, NCAR = No. of real roots stored in array CAR.) NCA, NCB,  
 NCC, NCD; NCE, NCF, NDD, NDE, NDF, NCAC, NCAR, NDCL

e) Logical constants used for TJET

A logical constant is TRUE if the expression to the right of the colon (:) is true; FALSE, otherwise.

Symbols:  $a|b$  means a or b;  $a\&b$  means a and b.

LA:	$NWNA > 0$	Speed Control loop closed
LAN:	$NWNA \leq 0$	Speed Control loop open
LB:	$NAT > 0$	Temperature Control loop closed
LBN:	$NAT \leq 0$	Temperature Control loop open
LC:	$NNT > 0$	$K_{NT} \neq 0$
LCN:	$NNT \leq 0$	No decoupling gain $K_{NT}$
LD:	$NTN > 0$	$K_{TN} \neq 0$

Table II. Concluded

LDN:	$NTN \leq 0$	No decoupling gain $K_{TN}$
LEN:	$K_{N2A} = 0$	No integrator in speed loop
LFN:	$K_{T6A} = 0$	No integrator in temperature loop
LH:	$(LEN \& LFN)   (LAN \& LFN)   (LBN \& LEN)   (LAN \& LBN)$ If LH is true, then a free s term exists.	
LAC:	$LA   LC$	Speed loop closed or $K_{NT} \neq 0$
LAD:	$LA   LD$	Speed loop closed or $K_{TN} \neq 0$
LBC:	$LB   LC$	Temperature loop closed or $K_{NT} \neq 0$
LBD:	$LB   LD$	Temperature loop closed or $K_{TN} \neq 0$
LIN:	$(W_{FX} = 0)   (P_{4X} = 0)$	No $P_{4X}$ term, see equations.
LP:	$CPO = 1.$	If true, then print-out provided for checkout of program

#### FORMAT OF INPUT DATA FOR TJET

The following pages (Table IV) show the format of input data for TJET. The data cards should follow the [//G . SYSIN DD \*] control card and should be arranged as follows:

1. Title card, description of run in alpha-numeric characters which will be printed on top of first page of run. This card must be first card of each run.
2. Data cards for each run. All data must be Real \*4 and are read into array F of main program TJET. Relative locations of the variables assigned to array F are described on the following data sheets. Blanks will leave data from previous run unchanged. A minus sign must be in Column 1 on last data card of each run.

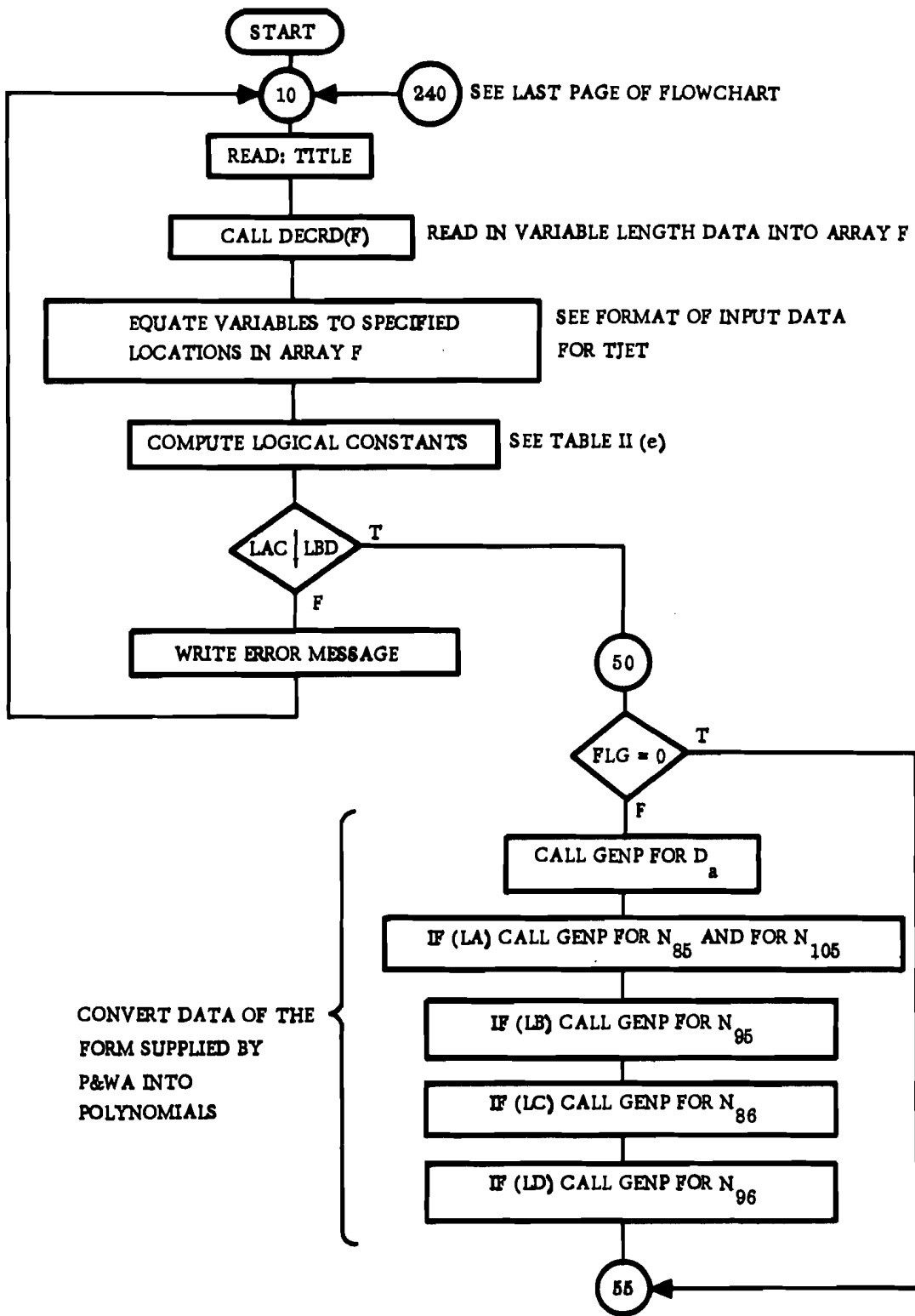


Figure 3. Flowchart of Main Program TJET

COMPUTE  
DENOMINATOR  
FOR ROOT LOCUS

COMPUTE  
NUMERATOR  
FOR SPEED  
LOOP CLOSURE

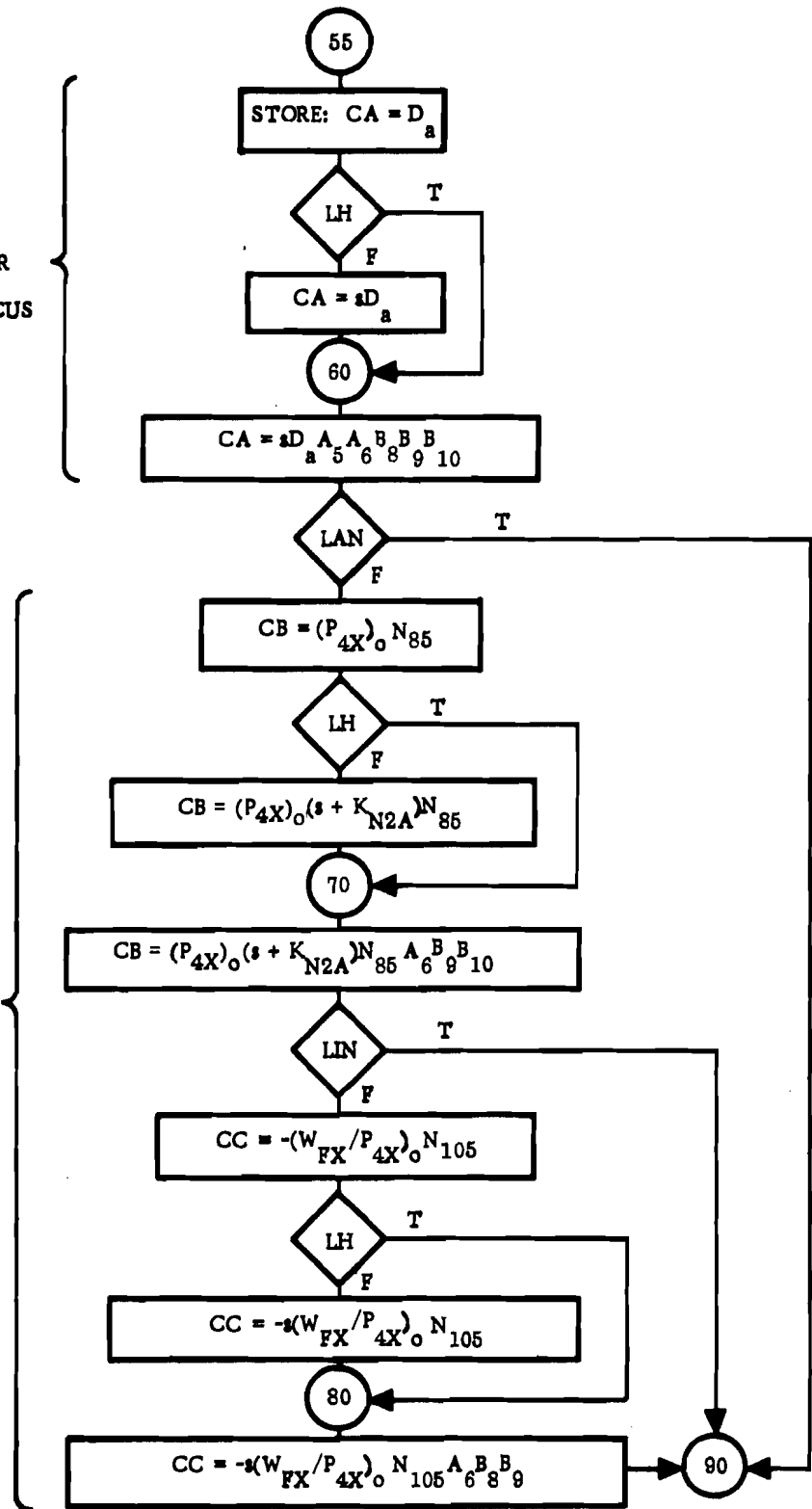


Figure 3. (Continued)

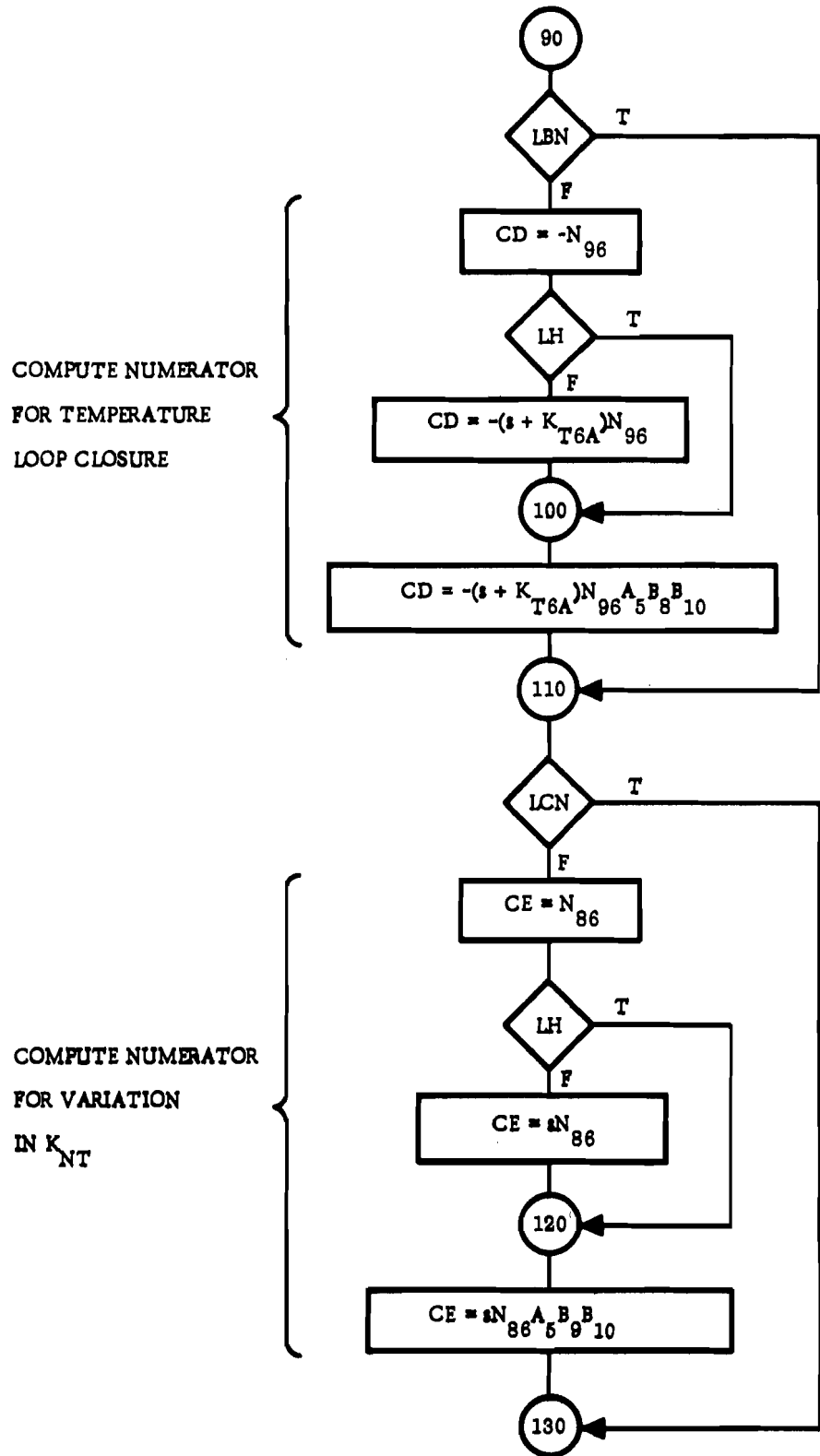


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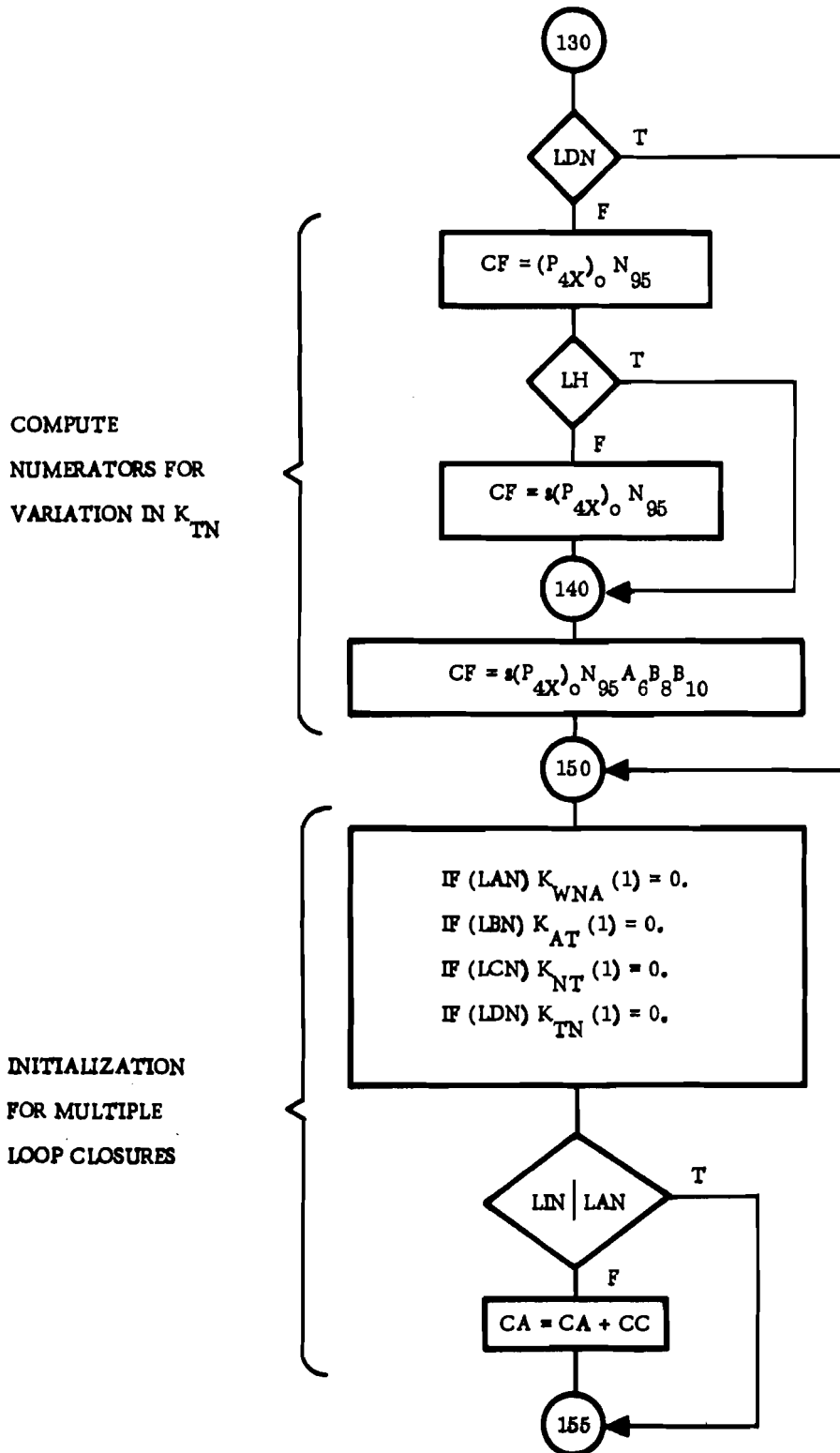


Figure 3. (Continued)



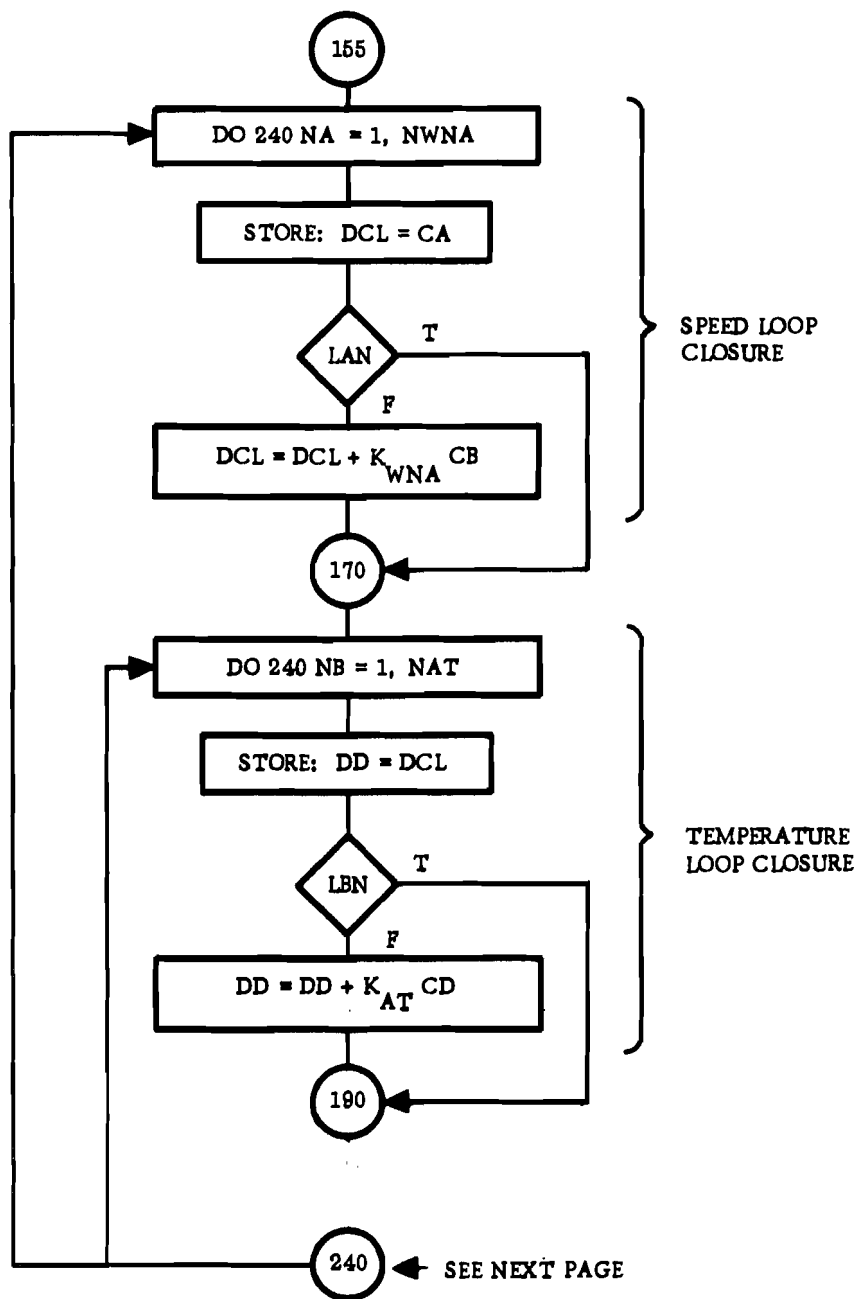


Figure 3. (Continued)

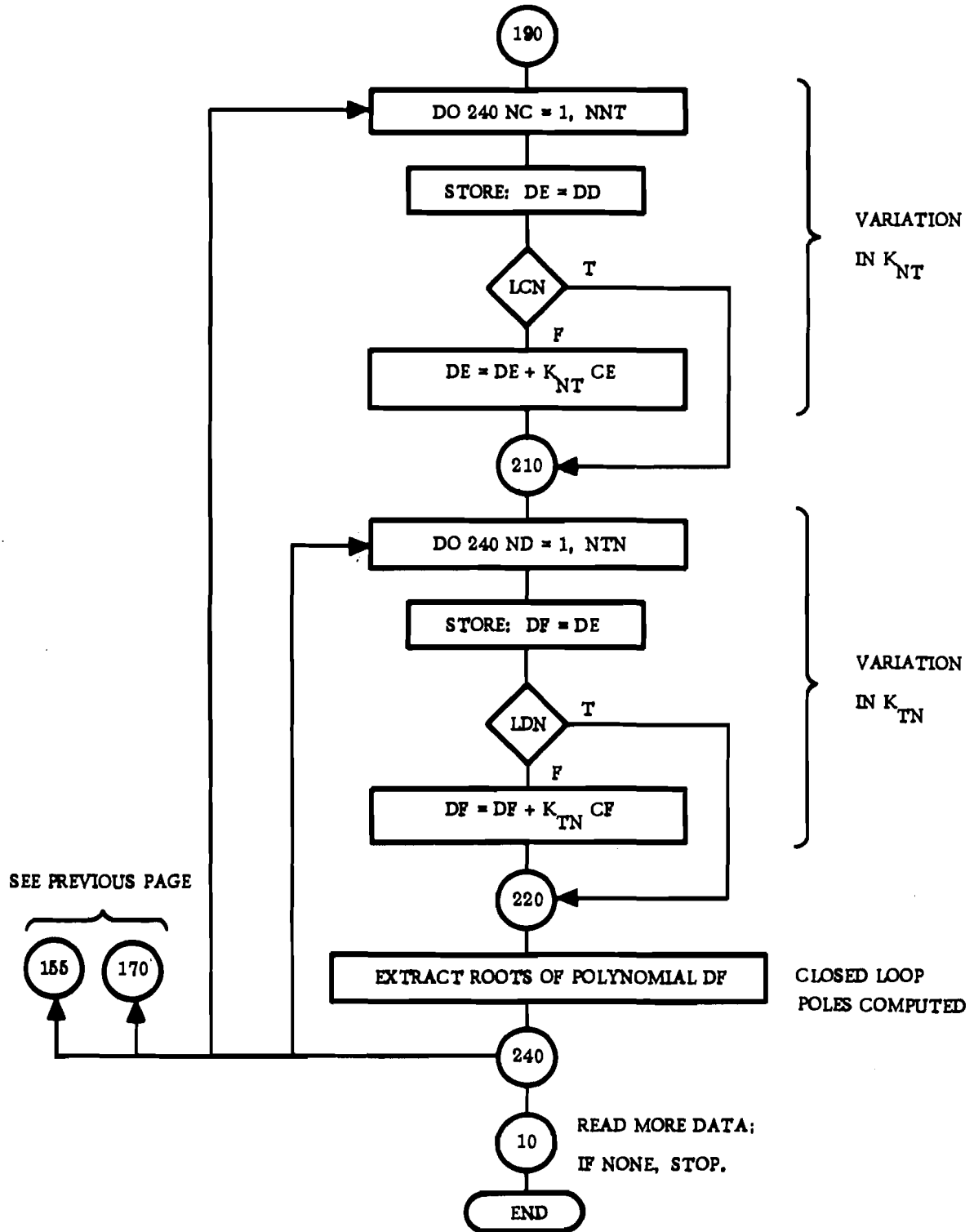


Figure 3. (Concluded)

Table III. Fortran H Program Listing of TJET

C	MAIN PROGRAM	00000030
C	ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR TURBOJET ENGINE	00000040
C	DEVELOPED BY E.L.LUM FEBRUARY 1968	00000050
C		00000060
	IMPLICIT LOGICAL*4(L)	00000070
	COMPLEX*8 CAC(10)	00000080
	REAL*4 DA(8),N85(8),N86(8),N95(8),N96(8),N105(8)	00000090
	REAL*4 KWNA(19),KAT(19),KNT(19),KTN(19),KN2A,KT6A	00000100
	REAL*4 TA5(4),TA6(4),TB9(4),TB10(4),TITLE(18),F(170),TB8(4)	00000110
	REAL*4 CA(20),CB(20),CC(20),CD(20),CE(20),CF(20),CAR(20)	00000120
	REAL*4 DCL(20),DD(20),DE(20),DF(20)	00000130
	COMMON /CMB/TA5,TA6,TB8,TB9,TB10,NTA5,NTA6,NTB8,NTB9,NTB10	00000145
	EQUIVALENCE (F(2),DA),(F(12),N85),(F(22),N86),(F(32),N95),	00000150
	1(F(42),N96),(F(52),N105),(F(61),P4A),(F(62),WFA),(F(63),KN2A),	00000160
	2(F(64),KT6A),(F(65),CPO),(F(67),KWNA),(F(87),KAT),(F(107),KNT),	00000170
	3(F(127),KTN),(F(10),FLG),(F(20),G85),(F(30),G86),(F(40),G95),	00000180
	4(F(50),G96),(F(60),G105)	00000185
	SF=1.	00000190
	DO 5 I=1,170	00000194
	5 F(I)=0.	00000196
	10 READ(5,20)TITLE	00000200
	20 FORMAT(18A4)	00000210
	WRITE(6,25)TITLE	00000220
	25 FORMAT(1H1,4X,'ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR TURBOJET	00000230
	1 ENGINE'//5X,18A4)	00000240
	CALL DECRO(F)	00000250
	WRITE(6,30)	00000260
	30 FORMAT(1H0,4X,'NON-ZERO INPUT DATA'//4(10X,'I',7X,'F(I)',5X))	00000270
	CALL PRIN(F,170)	00000280
	DO 35 I=1,4	00000282
	TA5(I)=F(I+146)	00000283
	TA6(I)=F(I+151)	00000284
	TB8(I)=F(I+166)	00000285
	TB9(I)=F(I+156)	00000286
	35 TB10(I)=F(I+161)	00000287
	NDA=F(1)	00000290
	NN85=F(11)	00000300
	NN86=F(21)	00000310
	NN95=F(31)	00000320

Table III. (Continued)

NN96=F(41)	00000330
NN105=F(51)	00000340
NNNA=F(66)	00000350
NAT=F(86)	00000360
NNT=F(106)	00000370
NTN=F(126)	00000380
NTA5=F(146)	00000390
NTA6=F(151)	00000400
NTB9=F(156)	00000410
NTB10=F(161)	00000420
NTB8=F(166)	00000425
CAR(1)=1.	00000427
LA=NNNA.GT.0	00000430
LAN=NOT.LA	00000440
LB=NAT.GT.0	00000450
LBN=NOT.LB	00000460
LC=NNT.GT.0	00000470
LCN=NOT.LC	00000480
LD=NTN.GT.0	00000490
LDN=NOT.LD	00000500
LEN=KN2A.EQ.0.	00000510
LFN=KT6A.EQ.0.	00000520
LH=LEN.AND.LFN.OR.LAN.AND.LFN.OR.LBN.AND.LEN.OR.LAN.AND.LBN	00000530
LAC=LA.OR.LC	00000540
LAD=LA.OR.LD	00000550
LBC=LB.OR.LC	00000560
LBD=LB.OR.LD	00000570
LIN=MFA.EQ.0..OR.P4A.EQ.0.	00000590
LP=.TRUE.	00000600
IF(LAC.OR.LBD)GO TO 50	00000640
WRITE(6,40)	00000650
40 FORMAT(1H0,4X,'OPEN LOOP, NO CONTROL GAINS SPECIFIED')	00000660
GO TO 10	00000670
50 IF(FLG.EQ.0.)GO TO 55	00000672
WRITE(6,52)	00000674
52 FORMAT(1H0,2X,'OPEN LOOP TRANSFER FUNCTION POLYNOMIALS GENERATED')	00000676
CALL GENP(DA,ND A,1.,'DA(S) ',2)	00000678
IF(LA)CALL GENP(NB5,NNB5,G85,'NB5(S) ',2)	00000680
IF(LC)CALL GENP(NB6,NNB6,G86,'NB6(S) ',2)	00000682
IF(LD)CALL GENP(NB5,NNB5,G95,'NB5(S) ',2)	00000684

Table III. (Continued)

	IF(LB)CALL GENP(N96,NN96,G96,'N96(S) ',2)	00000686
	IF(LA)CALL GENP(N105,NN105,G105,'N105(S) ',2)	00000688
C	COMPUTE DENOMINATOR CA(S)	00000694
55	CALL GPOL(DA,NDA,1.,CA,NCA)	00000696
	IF(LH)GO TO 60	00000700
	NCA=NCA+1	00000710
	CA(NCA+1)=0.	00000720
60	CALL XPNP5(CA,NCA,LAD,LBC,LAC,LBD,LA,'OPEN LOOP DENOMINATOR, CA(S)	00000740
	1',7,'OPEN LOOP POLES ',4,&10)	00000750
	IF(LAN)GO TO 90	00000790
	WRITE(6,310)	00000795
310	FORMAT(1H0,1X,'SPEED LOOP CLOSED')	00000800
	CALL GPOL(N85,NN85,P4A,CB,NCB)	00000810
	IF(LFN)WRITE(6,350)	00000814
350	FORMAT(1H0,4X,'NO INTEGRATOR IN SPEED LOOP')	00000816
	IF(LH)GO TO 70	00000820
	WRITE(6,370)KN2A	00000830
370	FORMAT(1H0,4X,'INTEGRATOR GAIN, KN2A=',G12.5)	00000835
	CAR(2)=KN2A	00000840
	CALL POLYX(CB,NCB,CAR,1,CB,NCB)	00000850
70	CALL XPNP5(CB,NCB,,FALSE.,LBC,,FALSE.,LBD,LA,'NUMERATOR ASSOCIATED	00000860
	1 WITH KWNA, CB(S) ',10,'ZEROS ASSOCIATED WITH KWNA ',7,&10)	00000870
	IF(LIN)GO TO 90	00000915
	CALL GPOL(N105,NN105,-WFA/P4A,CC,NCC)	00000920
	IF(LH)GO TO 80	00000930
	NCC=NCC+1	00000940
	CC(NCC+1)=0.	00000950
80	CALL XPNP5(CC,NCC,,FALSE.,LBC,LAC,LBD,LAN,'NUMERATOR ASSOCIATED WI	00000960
	1TH P4A, CC(S) ',9,'ZEROS ASSOCIATED WITH P4A ',7,&10)	00000970
90	IF(LBN)GO TO 110	00001010
	WRITE(6,320)	00001015
320	FORMAT(1H0,1X,'TEMPERATURE LOOP CLOSED')	00001020
	CALL GPOL(N96,NN96,-1.,CD,NCD)	00001030
	IF(LFN)WRITE(6,360)	00001034
360	FORMAT(1H0,4X,'NO INTEGRATOR IN TEMPERATURE LOOP')	00001036
	IF(LH)GO TO 100	00001040
	WRITE(6,380)KT6A	00001050
380	FORMAT(1H0,4X,'INTEGRATOR GAIN, KT6A=',G12.5)	00001055
	CAR(2)=KT6A	00001060
	CALL POLYX(CD,NCD,CAR,1,CD,NCD)	00001070

Table III. (Continued)

100	CALL XPNP5(CD,NCD,LAD,,FALSE,,LAC,,FALSE,,LA,'NUMERATOR ASSOCIATED	00001080
	1 WITH KAT, CD(S)',9,'ZEROS ASSOCIATED WITH KAT ',7,&10)	00001090
110	IF(LCN)GO TO 130	00001130
	WRITE(6,330)	00001135
330	FORMAT(1H0,1X,'VARIATION IN KNT')	00001140
	CALL GPOL(N86,NN86,1.,CE,NCE)	00001150
	IF(LH)GO TO 120	00001160
	NCE=NCE+1	00001170
	CE(NCE+1)=0.	00001180
120	CALL XPNP5(CE,NCE,LAD,,FALSE,,FALSE,,LBD,LA,'NUMERATOR ASSOCIATED	00001190
	1 WITH KNT, CE(S)',9,'ZEROS ASSOCIATED WITH KNT ',7,&10)	00001200
130	IF(LDN)GO TO 150	00001250
	WRITE(6,340)	00001255
340	FORMAT(1H0,1X,'VARIATION IN KTN')	00001260
	CALL GPOL(N95,NN95,P4A,CF,NCF)	00001270
	IF(LH)GO TO 140	00001280
	NCF=NCF+1	00001290
	CF(NCF+1)=0.	00001300
140	CALL XPNP5(CF,NCF,,FALSE,,LBC,LAC,,FALSE,,LA,'NUMERATOR ASSOCIATED	00001310
	1 WITH KTN, CF(S)',9,'ZEROS ASSOCIATED WITH KTN ',7,&10)	00001320
C	MULTIPLE LOOP CLOSURES	00001360
150	IF(LAN)KWNA(1)=0.	00001370
	IF(LBN)KAT(1)=0.	00001380
	IF(LCN)KNT(1)=0.	00001390
	IF(LDN)KTN(1)=0.	00001400
	LP=CPD.EQ.1.	00001402
	IF(LIN.OR.LAN)GO TO 155	00001410
	CALL POLADD(CC,NCC,1.,CA,NCA,1.,CA,NCA)	00001415
	CALL WRTPOL(CA,NCA,'CA=CA+CC',2)	00001420
155	WRITE(6,160)TITLE	00001425
160	FORMAT(1H1,4X,18A4//75X,'BEGIN LOOP CLOSURES')	00001430
	DO 240 NA=1,NWNA	00001435
	CALL GPOL(CA,NCA,1.,DCL,NDCL)	00001437
	IF(LAN)GO TO 170	00001440
	CALL POLADD(CB,NCB,KWNA(NA),DCL,NDCL,1.,DCL,NDCL)	00001450
170	DO 240 NB=1,NAT	00001470
	CALL GPOL(DCL,NDCL,1.,DD,NDD)	00001500
	IF(LBN)GO TO 190	00001505
	CALL POLADD(CD,NCD,KAT(NB),DD,NDD,1.,DD,NDD)	00001510
190	DO 240 NC=1,NNT	00001530

Table III. (Concluded)

CALL GPOL(DD,ND,1.,DE,NDE)	00001550
IF(LCN)GO TO 210	00001560
CALL POLADD(CE,NCE,KNT(NC),DE,NDE,1.,DE,NDE)	00001580
210 DD 240 ND=1,NTN	00001600
CALL GPOL(DE,NDE,1.,DF,NDF)	00001620
IF(LDN)GO TO 220	00001640
CALL POLADD(CF,NCF,KTN(ND),DF,NDF,1.,DF,NDF)	00001650
220 WRITE(6,230)KWNA(NA),KAT(NB),KNT(NC),KTN(ND)	00001660
230 FORMAT(1H0// ' CONTROL GAINS: KWNA=',G12.5,' , KAT=',G12.5,' , KNT='	00001670
1,G12.5,' , KTN=',G12.5)	00001680
IF(LP)CALL WRTPOL(DF,NDF,'CLOSED LOOP DENOMINATOR ',6)	00001690
CALL PRTX (DF,NDF,CAR,NCAR,CAC,NCAC,50,1.E6,SF,&10)	00001700
240 CALL WRT(CAR,NCAR,CAC,NCAC,'CLOSED LOOP POLES ',5)	00001710
WRITE(6,260)	00001810
260 FORMAT(1H0,4X,'END OF LOOP CLOSURES')	00001820
GO TO 10	00001830
END	00001840



Table IV. Input Data Format for TJET

DECK NO. TJET PROGRAMMER E. L. LUM DATE 5-29-68 PAGE 1 of 5 JOB NO. \_\_\_\_\_

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1		Must be first card of run.
13		
25		
37		
49		
61		
1	Identification	
13	1	Relative data field location in array F of main program TJET.
25	NDA	1 Degree of open-loop denominator polynomial
37	DA(1) Variable names assigned to data	2 Open-loop denominator polynomial, Da(s)
49	DA(8) fields shown	9 See special instructions
61	FLG	10 See special instructions on previous page.
1	1 1	
13	NN85	11 Degree of numerator $N_{85}(s)$
25	N85(1)	12 Numerator polynomial $N_{85}(s) = \partial N_{2X} / \partial W_{XX}$ for Speed Control
37		See special instructions
49	N85(8)	19
61	G85	20 Gain of $N_{85}(s)$ , used only if FLG $\neq$ 0.
1	2 1	
13	NN86	21 Degree of numerator $N_{86}(s)$
25	N86(1)	22 Numerator polynomial $N_{86}(s) = \partial N_{2X} / \partial A_{XX}$
37		See special instructions
49	N86(8)	29
61	G86	30 Gain of $N_{86}(s)$ , used only if FLG $\neq$ 0.

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Table IV. (Cont)

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 3 of 5 JOB NO. \_\_\_\_\_

	NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1		3 1	
13	NN95		31 Degree of numerator $N_{95}(s)$
25	N95(1)		32 Numerator polynomial $N_{95}(s) = \partial T_{6X} / \partial W_{FX}$
37	↓		See special instructions
49	N95(8)		39
61	G95		40 gain of $N_{95}(s)$ , used only if $FLG \neq 0$ .
1		4 1	
13	NN96		41 Degree of numerator $N_{96}(s)$
25	NN96(1)		42 Numerator polynomial $N_{96}(s) = \partial T_{6X} / \partial A_{3X}$ , for Temperature Control
37	↓		See special instructions
49	N96(8)		49
61	G96		50 gain of $N_{96}(s)$ , used only if $FLG \neq 0$
1		5 1	
13	NN105		51 Degree of numerator $N_{105}(s)$
25	N105(1)		52 Numerator polynomial $N_{105}(s) = \partial P_{4X} / \partial W_{FX}$
37	↓		See special instructions
49	N105(8)		59
61	G105		60 gain of $N_{105}(s)$ , used only if $FLG \neq 0$ .
1		6 1	
13	P4A		61 $(P_{4X})_0$ , initial steady state value of $P_{4X}$
25	WFA		62 $(W_{FX})_0$ , initial steady state value of $W_{FX}$
37	KN2A		63 $K_{N2A}$ , integrator gain in Speed Control loop
49	KT6A		64 $K_{T6A}$ , integrator gain in Temperature Control loop
61	CPO		65 Check-out print option, 1. if print-out desired

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Table IV. (Cont)

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 3 of 5 JOB NO. \_\_\_\_\_

	NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	6 6		
13	NWNA		66 No. of Control gains, $K_{WNNA}$ ; 0. if Speed Control loop open
23	KWNA(1)		67
37	↓		} Set of control gains $K_{WNNA}$ for Speed Control loop
49	↓		
61	KWNA(19)	73 80	85 } closure for which closed-loop characteristic is computed.
1	8 6		
13	NAT		86 No. of Control gains, $K_{AT}$ ; 0. if Temperature Control loop open
23	KAT(1)		87
37	↓		} Set of control gains $K_{AT}$ for Temperature Control
49	↓		
61	KAT(19)	73 80	105 } loop closure for which closed loop characteristic is computed.
1	1 0 6		
13	NNT		106 No. of decoupling gains $K_{NT}$
23	KNT(1)		107
37	↓		} Set of decoupling gains $K_{NT}$ for
49	↓		
61	KNT(19)	73 80	125 } which closed loop characteristic is computed.
1	1 2 6		
13	NTN		126 No. of decoupling gains $K_{TN}$
23	KTN(1)		127
37	↓		} Set of decoupling gains $K_{TN}$ for
49	↓		
61	KTN(19)	73 80	145 } which closed loop characteristic is computed.

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Table IV. (Cont)

DECK NO. \_\_\_\_\_ PROGRAMMER \_\_\_\_\_ DATE \_\_\_\_\_ PAGE 4 of 5 JOB NO. \_\_\_\_\_

	NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	1 4 6		
13	NTA5		146 No. of time constants for $A_5$
25	TA5(1)		147 )
37	↓		148 Set of time constants for
49	↓	73 .80	149 $W_{PX}$ actuator lags, $1/A_5$
61	TA5(4)		150 )
1	1 5 1		
13	NTA6		151 No. of time constants for $A_6$
25	TA6(1)		152 )
37	↓		153 Set of time constants for
49	↓	73 .80	154 $A_{JX}$ actuator lags, $1/A_6$
61	TA6(4)		155 )
1	1 5 6		
13	NTB9		156 No. of time constants for $B_9$
25	TB9(1)		157 )
37	↓		158 Set of time constants for
49	↓	73 .80	159 $T_{GX}$ sensor lags, $1/B_9$
61	TB9(4)		160 )
1	1 6 1		
13	NTB10		161 No. of time constants for $B_{10}$
25	TB10(1)		162 )
37	↓		163 Set of time constants for
49	↓	73 .80	164 $P_{4X}$ sensor lags, $1/B_{10}$
61	TB10(4)		165 )

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Table IV. (Concluded)

DECK NO. TJET PROGRAMMER E. L. LUM DATE 5-29-68 PAGE 5 of 5 JOB NO. \_\_\_\_\_

NUMBER		IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	-		
13	1 6 6		
25	NTB8		166 No. of time constants for $B_0$
37	TB8(1)		167
49	↓		168 Set of time constants for
61	TB8(4)	73 80	169 } $N_{2X}$ sensor lags, $1/B_0$
			170
1			
13	Title card for next run		
25			
37			
49		73 80	
61			
1	-		
13	x x x		
25	Last card of next run		
37			
49		73 80	
61			
1	/ *		This card must be last card of entire deck
13			
25			
37			
49		73 80	
61			

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a. Special instructions for data entered into locations 2 through 9, 12 through 19, 22 through 29, 32 through 39, 42 through 49, and 52 through 59 (transfer function data):

- (1) If FLG (location 10) = 0, then these locations contain the coefficients of the indicated polynomials.
- (2) If FLG  $\neq$  0, then these locations contain the first-order lags,  $\omega_i$ , of the form supplied by P&WA, that is,

$$p(s) = g(1 + s/\omega_1) (1 + s/\omega_2) \dots (1 + s/\omega_n)$$

where  $g$  is the steady state gains of  $p(s)$ . The  $\omega_i$  's are destroyed by the program, and for the next run, these locations will contain the coefficients of the computed polynomial  $p(s)$ .

3. Repeat 1 and 2 above for as many runs as necessary.
4. Last card of entire deck must contain/\* in Columns 1 and 2.

#### EXAMPLE CASE USING TJET

The example case used is for a turbojet engine operating at sea level, Mach 0.8, military power setting. The necessary transfer functions polynomials required for the Speed Control are:

$$\begin{aligned} D_a &= -0.554335s^2 - 95.0994s - 337.734 \\ &= -0.554335 (s + 3.62811) (s + 167.928) \end{aligned}$$

$$N_{85} = -5.55574s - 1883.08 = -5.55574 (s + 338.943)$$

$$\begin{aligned} N_{105} &= -15.4052s^2 - 2674.94s - 20258.1 \\ &= -15.4052 (s + 7.9360) (s + 165.702) \end{aligned}$$

The actuator and sensor lags are:

$$A_5 = 0.02 (s + 50)$$

$$B_8 = 0.05 (s + 20)$$

$$B_{10} = 0.02 (s + 50)$$

The initial conditions are:

$$(P_{4X})_0 = 380.58 \text{ psia}$$

$$(W_{FX})_0 = 3.92222 \text{ lb/sec}$$

The integrator gain is set to  $K_{N2A} = 1.0 \text{ sec}^{-1}$ .

For the speed loop closure only, we set  $K_{AT} = K_{NT} = K_{TN} = 0$ .

The following computer print-out (Table V) shows the computation of the closed loop characteristic and poles for the speed loop closure, for control gain  $K_{WNA}$  varying between 0.0 and 0.05. A plot of the root locus of the closed loop poles are shown on Figure 4.



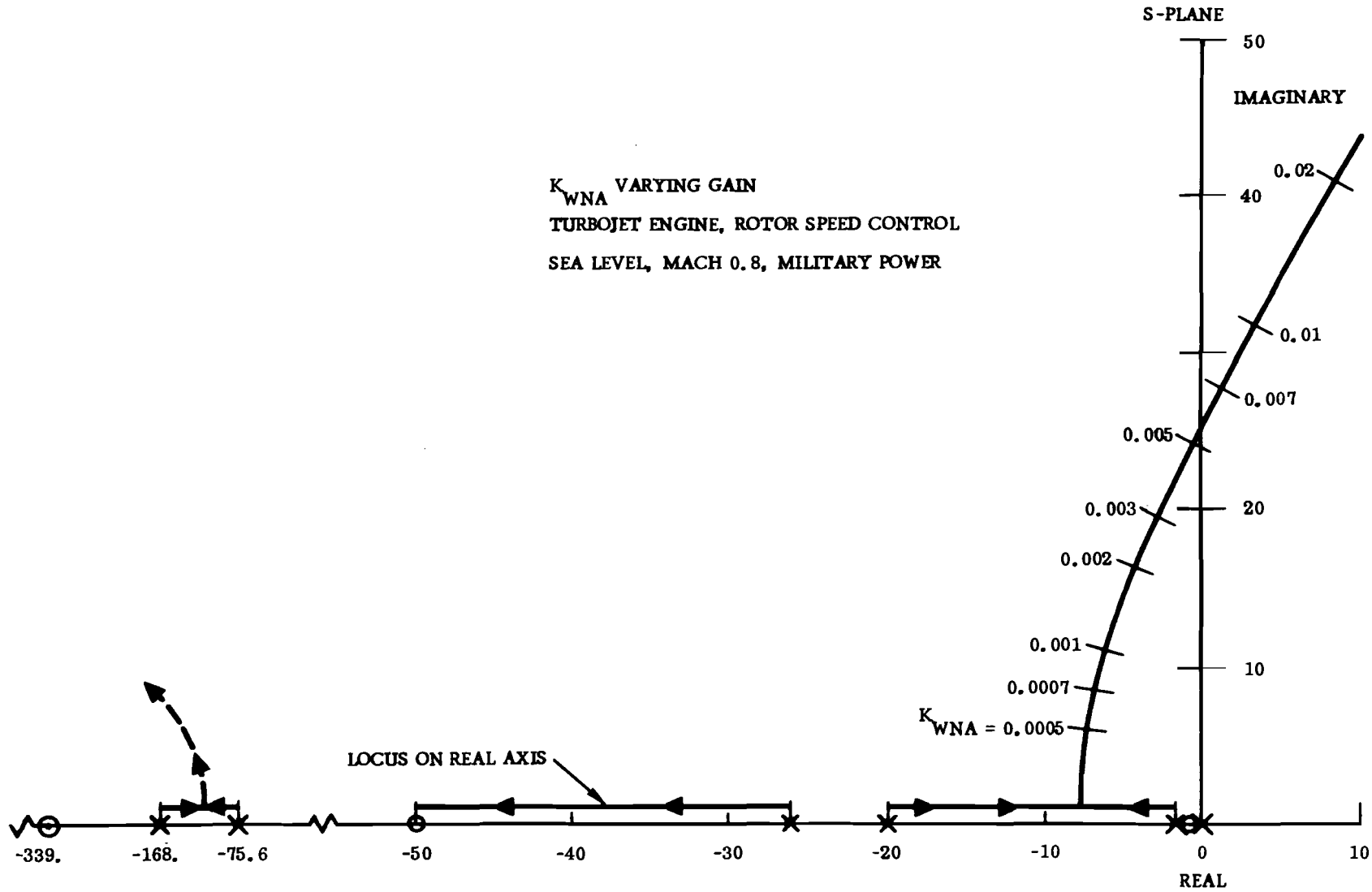


Figure 4. Root Locus for Example Case Using TJET

Table V. Computer Printout for Example Case Using TJET

ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR SATELLITE ENGINE

TURBOJET, MIL POWER, H=0, M=0.8, SPEED LOOP CLOSURE ONLY

NON-ZERO INPUT DATA SEE FORMAT OF INPUT DATA

I	F(I)	I	F(I)	I	F(I)	I	F(I)
1	2.00000	2	-0.554335	3	-95.0994	4	-337.734
11	1.00000	12	-5.55574	13	-1883.08	22	-61.5205
31	2.00000	32	-168.621	33	-25573.8	34	-65030.0
41	1.00000	42	212.246	43	1613.31	51	2.00000
52	-15.4052	53	-2674.94	54	-20258.1	61	380.580
62	3.92222	63	1.00000	64	5.00000	65	1.00000
66	19.0000	68	0.200000E-04	69	0.300000E-04	70	0.500000E-04
71	0.700000E-04	72	0.100000E-03	73	0.200000E-03	74	0.300000E-03
75	0.500000E-03	76	0.700000E-03	77	0.100000E-02	78	0.200000E-02
79	0.300000E-02	80	0.500000E-02	81	0.700000E-02	82	0.100000E-01
83	0.200000E-01	84	0.300000E-01	85	0.500000E-01	91	0.300000E-03
92	0.500000E-03	93	0.700000E-03	94	0.100000E-02	95	0.200000E-02
96	0.300000E-02	97	0.500000E-02	98	0.700000E-02	99	0.100000E-01
100	0.200000E-01	101	0.300000E-01	102	0.500000E-01	103	0.700000E-01
104	0.100000E 00	105	0.200000	146	1.00000	147	0.200000E-01
151	1.00000	152	0.200000E-01	156	1.00000	157	1.00000
161	1.00000	162	0.200000E-01	166	1.00000	167	0.500000E-01

OPEN LOOP DENOMINATOR, CA(S)

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04	-0.323239E-02	-0.284883	-9.92384	-125.495
-337.734	0.0			

OPEN LOOP POLES

NUMBER OF REAL ROOTS= 6

-3.62811	-19.9999	-50.0001	-50.0002	-167.928
0.0				

Compute open-loop denominator for speed loop closure

SPEED LOOP CLOSED

INTEGRATOR GAIN, KN2A= 1.0000

NUMERATOR ASSOCIATED WITH KWNA, CB(S)

POLYNOMIAL OF ORDER 3, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-42.2880	-16489.9	-733110.	-716662.
----------	----------	----------	----------

Compute numerators for speed loop closure

ZEROS ASSOCIATED WITH KWNA

Table V. (Continued)

NUMBER OF REAL ROOTS= 3					} Compute numerators for speed loop closure
-50.0000	-1.00000	-338.943			
NUMERATOR ASSOCIATED WITH P4A, CC(S)					
POLYNOMIAL OF ORDER 4, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE					
0.793825E-02	1.53715	38.0065	208.778	0.0	
ZEROS ASSOCIATED WITH P4A					
NUMBER OF REAL ROOTS= 4					
-20.0000	-7.93600	-165.702	0.0		
CA=CA+CC					
POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE					
-0.110867E-04	-0.323239E-02	-0.276945	-8.38669	-87.4889	
-128.957	0.0				

Table V. (Continued)

SATELLITE, MIL POWER, H=0, M=0.8, SPEED LOOP CLOSURE ONLY

BEGIN LOOP CLOSURES

Variable Gain

All of these gains are set to zero.

CONTROL GAINS: KWNA= 0.0

KAT= 0.0 , KNT= 0.0 , KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

$(-0.110867E-04)s^6 - (0.323239E-02)s^5 - (0.276945)s^4 - (8.38669)s^3 - (87.4889)s^2$   
 $- (28.957)s + 0.0$

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-1.75134      -26.1284      -20.0001      -168.045      -75.6312  
 0.0

Check open-loop poles

CONTROL GAINS: KWNA= 0.20000E-04, KAT= 0.0

, KNT= 0.0

, KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

$-0.110867E-04 s^6 - 0.323239E-02 s^5 - 0.276945 s^4 - 8.38754 s^3 - 87.8187 s^2$   
 $- 143.619 s - 14.3332$

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-1.85717      -0.106690      -19.2933      -75.6579      -26.6006  
 -168.040

First gain change  
 $K_{WNA} = 0.00002$

CONTROL GAINS: KWNA= 0.30000E-04, KAT= 0.0

, KNT= 0.0

, KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

$-0.110867E-04 s^6 - 0.323239E-02 s^5 - 0.276945 s^4 - 8.38796 s^3 - 87.9836 s^2$   
 $- 150.950 s - 21.4999$

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-0.156493      -1.91675      -26.8064      -18.9667      -168.037

CS

Table V. (Continued)

-75.6720

CONTROL GAINS:  $K_{MNA} = 0.5000E-04$ ,  $K_{AT} = 0.0$  ,  $K_{NT} = 0.0$  ,  $K_{TN} = 0.0$

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04	-0.323239E-02	-0.276945	-8.38881	-88.3134
-165.612	-35.8331			

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-2.05030	-0.248536	-27.1777	-18.3476	-168.033
-75.6986				

CONTROL GAINS:  $K_{MNA} = 0.70000E-04$ ,  $K_{AT} = 0.0$  ,  $K_{NT} = 0.0$  ,  $K_{TN} = 0.0$

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04	-0.323239E-02	-0.276945	-8.38965	-88.6432
-180.274	-50.1664			

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-2.20417	-0.330248	-27.5069	-17.7607	-168.028
-75.7259				

CONTROL GAINS:  $K_{MNA} = 0.10000E-03$ ,  $K_{AT} = 0.0$  ,  $K_{NT} = 0.0$  ,  $K_{TN} = 0.0$

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04	-0.323239E-02	-0.276945	-8.39092	-89.1379
-202.268	-71.6662			

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 6

-0.433966	-2.47540	-27.9434	-16.9158	-168.021
-75.7663				

Table V. (Continued)

CONTROL GAINS: KWNA= 0.10000E-01, KAT= 0.0 , KNT= 0.0 , KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04    -0.323239E-02    -0.276945    -8.80957    -252.388  
 -7480.05    -7166.62

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 4  
 -0.992900    -88.0103    -43.6979    -165.499  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 3.32245    31.8092

CONTROL GAINS: KWNA= 0.20000E-01, KAT= 0.0 , KNT= 0.0 , KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04    -0.323239E-02    -0.276945    -9.23245    -417.287  
 -14791.2    -14333.2

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 4  
 -0.996455    -46.1716    -162.499    -98.6472  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 8.37923    41.0215

CONTROL GAINS: KWNA= 0.30000E-01, KAT= 0.0 , KNT= 0.0 , KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04    -0.323239E-02    -0.276945    -9.65533    -582.187  
 -22122.2    -21499.9

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 4  
 -0.997639    -47.2520    -158.772    -108.603  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 12.0348    47.3382

Table V. (Concluded)

CONTROL GAINS: KWNA= 0.50000E-01, KAT= 0.0 , KNT= 0.0 , KTN= 0.0

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 6, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

-0.110867E-04	-0.323239E-02	-0.276945	-10.5011	-911.985
-36784.4	-35833.1			

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 4

-0.998584	-48.2449	-141.754	-135.568
-----------	----------	----------	----------

NUMBER OF COMPLEX PAIR ROOTS= 1

17.5046	56.4327
---------	---------

END OF LOOP CLOSURES

### III. DESCRIPTION OF MAIN PROGRAM TFAN

#### BLOCK DIAGRAM AND NOMENCLATURE

The control systems for the turbofan under study are:

1. the turbofan low pressure rotor speed control, or Fan Speed Control, in short,
2. the fan discharge corrected air flow control, or Corrected Air Flow Control, in short,
3. the turbofan high pressure rotor speed control, or H. P. Rotor Speed Control, in short.

The block diagrams for the individual control loops are shown on Figure 5. The nomenclature used in the figure and in the control equations are defined by Table VI. Control gains  $K_{AN1}$ ,  $K_{AW}$ ,  $K_{WN2}$ ,  $K_{N1}$ ,  $K_W$ , and  $K_{N2}$  are to be determined by the linear analysis.

Program TFAN allows for the variation of control gains  $K_{AN1}$ ,  $K_{AW}$  or  $K_{WN2}$  to obtain the root locus of the corresponding control loop. Integrator gains  $K_{N1}$ ,  $K_W$  and  $K_{N2}$  are preselected. Individual control loops are investigated by setting the control gains for the other loops to zero. For example, to obtain a root locus for the Fan Speed Control only, one must let  $K_{AW} = K_{WN2} = 0$ .

The present version of TFAN is useful only for the analysis of single loop closures because the cross-coupling transfer functions necessary for the analysis of two or more coupled control loops were not included in the equations used in programming TFAN. This omission was made because the cross-coupling transfer functions for the turbofan engine were not available anyway. Hence, although TFAN is set up for sequential loop closures, the results for varying more than one control gain simultaneously will not be valid.

#### EQUATIONS FOR LINEAR ANALYSIS OF TURBOFAN ENGINE

The closed loop characteristic, (RC), of the turbofan engine control, without coupling between control loops, is (using the same notation as defined for the arrays in TFAN).

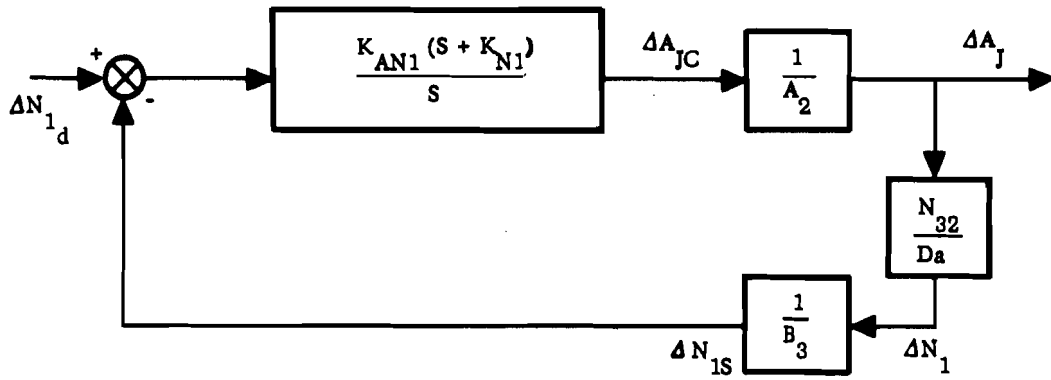
$$(RC) = (PA) + K_{AN1}(PB) + K_{AW}(PC) + [(PE) + K_{WN2}(PD)]$$

where

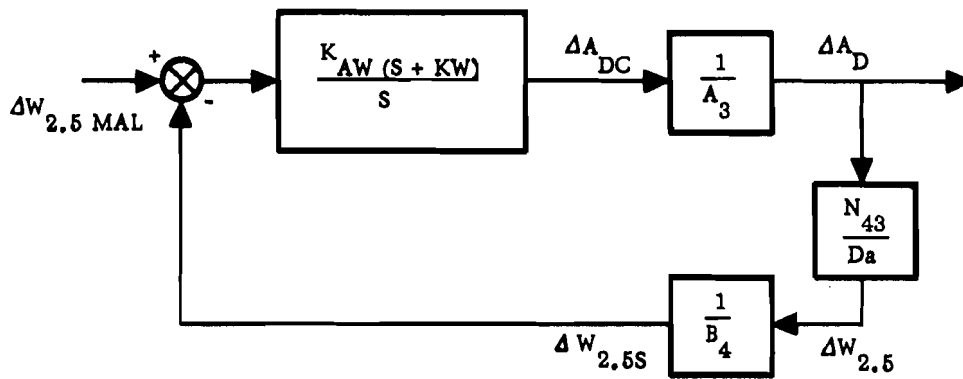
1. Denominator for root locus

$$(PA) = s(A_2B_3) (A_3B_4) (A_4B_5B_6B_7)D_a$$





(a) Fan Speed Control



(b) Fan Corrected Air Flow Control

Figure 5. Turbofan Engine Linear Control System Block Diagram

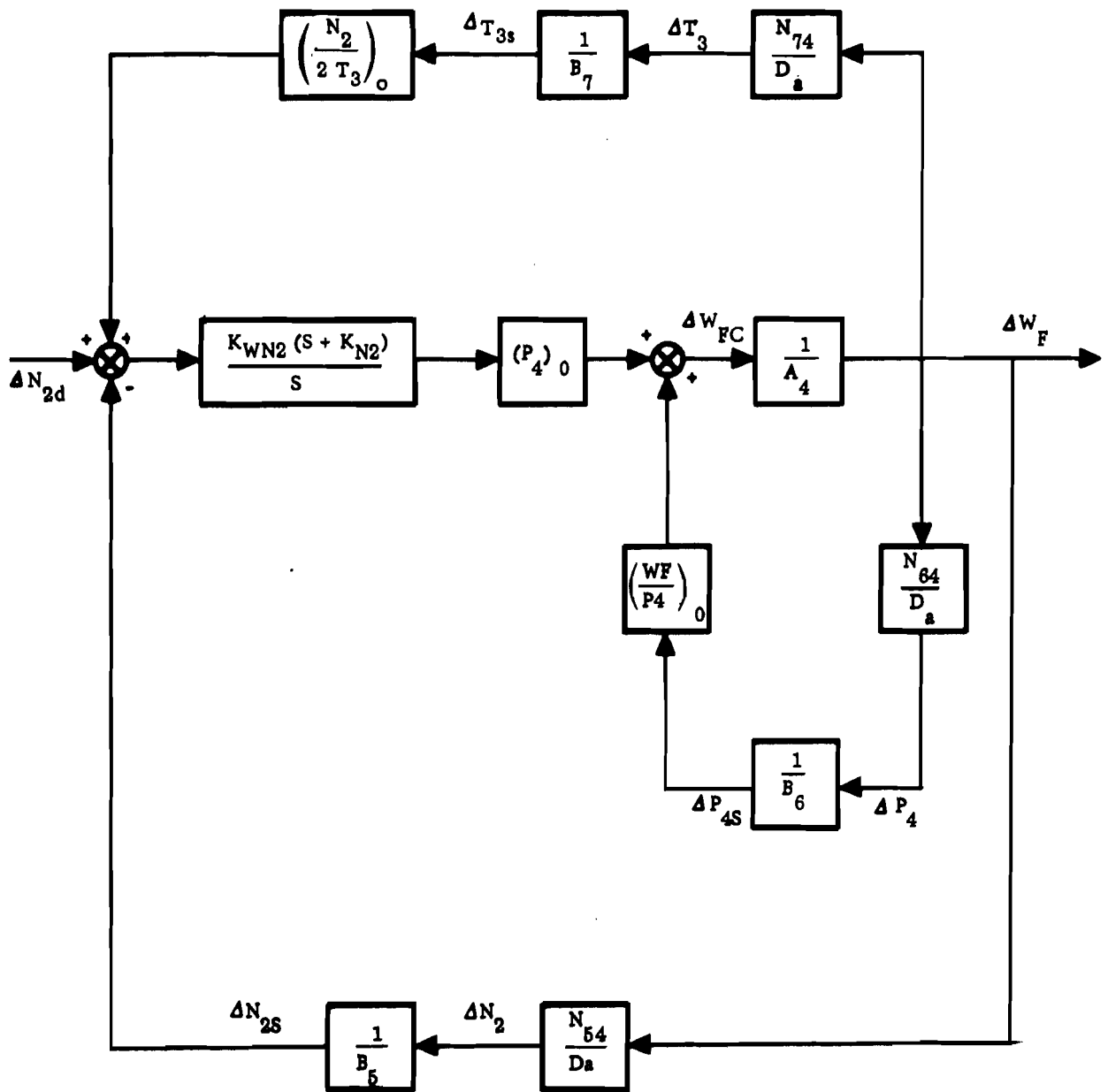


Figure 5. (Concluded)

Table VI. Nomenclature for Linear Analysis of Turbofan Engine Control

a) Actuated and Sensed Variables

Actuated Variables	Description
$x_2 = A_D$	Turbofan Main Exhaust Nozzle Area (ft <sup>2</sup> )
$x_3 = A_J$	Fan Duct Exhaust Nozzle Area (ft <sup>2</sup> )
$x_4 = W_F$	Turbofan Fuel Flow (lb/hr)
<b>Sensed Variables</b>	
$y_3 = N_1$	Fan Rotor Mechanical Speed (RPM)
$y_4 = W_{2.5}$	Fan Discharge Corrected Air Flow
$y_5 = N_2$	Turbofan High Pressure Rotor Mechanical Speed (RPM)
$y_6 = P_4$	Turbofan High Pressure Rotor Compressor Discharge Pressure (psia)
$y_7 = T_3$	Turbofan High Pressure Rotor Compressor Inlet Temperature (°R)

b) Actuator and Sensor Definitions

$A_J$	Actuator	=	$1/A_2$
$A_D$	Actuator	=	$1/A_3$
$W_F$	Actuator	=	$1/A_4$
$N_1$	Sensor	=	$1/B_3$
$W_{2.5}$	Sensor	=	$1/B_4$
$N_2$	Sensor	=	$1/B_5$
$P_4$	Sensor	=	$1/B_6$
$T_3$	Sensor	=	$1/B_7$

Table VI. Concluded

where  $A_j$  is the denominator of the actuator lag for  $x_j$ , and  $B_i$  is the denominator lag for  $y_i$ .

c) Transfer Function Numerators

$N_{32}$  = Numerator of  $\partial N_1 / \partial A_J$  Transfer Function

$N_{43}$  = Numerator of  $\partial W_{2.5} / \partial A_D$  Transfer Function

$N_{54}$  = Numerator of  $\partial N_2 / \partial W_F$  Transfer Function

$N_{64}$  = Numerator of  $\partial P_4 / \partial W_F$  Transfer Function

$N_{74}$  = Numerator of  $\partial T_3 / \partial W_F$  Transfer Function

In general,  $N_{ij}/D_a$  is the transfer function for the  $i$ -th dependent variable,  $y_i$ , due to the  $j$ -th independent variable  $x_j$ .  $D_a$  is the open loop denominator of the turbofan engine dynamics.

2. Numerator for Fan Speed Control

$$(PB) = N_{32}(s + K_{N1}) (A_3 B_4) (A_4 B_5 B_6 B_7)$$

3. Numerator for Corrected Air Flow Control

$$(PC) = N_{43}(s + K_W) (A_2 B_3) (A_4 B_5 B_6 B_7)$$

4. Numerators for H. P. Rotor Speed Control

$$(PD) = (s + K_{N2}) (P_4)_0 B_6 [N_{54} B_7 - (N_2 / 2T_3) N_{74} B_5] (A_2 B_3) (A_3 B_4)$$

$$(PE) = -s(W_F/P_4)_0 N_{64} (B_5 B_7) (A_2 B_3) (A_3 B_4)$$

Actually, TFAN has logic statements which omit certain actuator poles,  $A_i$ , and sensor poles,  $B_j$ , from these equations if they are not affected by one of the loop closures. For example, if only the Fan Speed Loop is closed, then  $(A_3 B_4)$  and  $(A_4 B_5 B_6 B_7)$  are set to unity.

## FLOWCHART AND PROGRAM LISTING OF TFAN

Table VII defines the nomenclature used in the programming of computer program TFAN. The flowchart for mainprogram TFAN is shown on Figure 6. The printout statements are left out of the flowchart for clarity. The circled numbers in Figure 6 correspond to the statement numbers in the Fortran H program listing of TFAN shown on Table VIII.

### FORMAT OF INPUT DATA FOR TFAN

The following pages (Table IX) show the format of input data for TFAN. The data cards should follow the [//G.SYSIN DD\*] control card and should be arranged as follows:

1. Title card, description of run in alpha-numeric characters which will be printed at top of first page of print-out of the run. This card must be the first card of each run.
2. Data cards for each run. All data must be real \*4 variables and are read into array F of main program TFAN. The relative locations of the variables assigned to array F are described on the following pages. Blanks will leave data from the previous run unchanged. A minus sign must be in Column 1 on the last data card for each run.
  - a. Special instructions for data entered into locations 2 through 9, 12 through 19, 22 through 29, 32 through 39, 42 through 49, and 52 through 59 (transfer function data):
    - (1) If FLG (location 10) = 0, then these locations contain the coefficients of the indicated polynomials.
    - (2) If FLG  $\neq$  0, then these locations contain the first-order lags,  $\omega_i$ , of the form supplied by P&WA, that is,

$$p(s) = g(1 + s/\omega_1) (1 + s/\omega_2) \dots (1 + s/\omega_n)$$

where  $g$  is the steady state gain of  $p(s)$ . The  $\omega_i$ 's are destroyed by the program, and for the next run these locations will contain the coefficients of the computed polynomial  $p(s)$ .

3. Repeat 1 and 2 above for as many runs as necessary.
4. The last card of the entire deck must contain/\* in Columns 1 and 2.

Table VII. List of Subprograms and Variables Used for TFAN

a) <u>List of Subprograms Required for TFAN</u>	
Non-library: in Fortran H for IBM 360	
1. XPNP3	Expand a polynomial with three sets of first-order lags
2. GENP	Generate a polynomial from data of the form given by P&WA
3. XPNTAU	Expand a polynomial with a given set of first-order lags
4. PRTX <sup>4</sup>	Polynomial root extraction using Bairstow and Newton-Raphson iteration algorithms
5. FLIP <sup>4</sup>	Reverse order of elements in an array
6. POLYX <sup>5</sup>	Multiply two polynomials
7. GPOL <sup>5</sup>	Multiply a polynomial by a constant
8. POLADD <sup>5</sup>	Add two polynomials
9. WRT <sup>5</sup>	Print roots of a polynomial
a. WRTPOL <sup>5</sup>	Print coefficients of a polynomial
10. PRIN <sup>5</sup>	Print non-zero elements of an array
11. STREAL <sup>5</sup>	Store two arrays in one array
a. STR3 <sup>5</sup>	Store three arrays in one array
Library: for Fortran IV on IBM 360	
12. DECRD	Read variable length data in standard format
<sup>4</sup> Developed by J. C. Long of NAR/Space Division.	
<sup>5</sup> Subprograms originally developed for ALODES's I and II, Automatic Linear Optimal Design and Evaluation, computer programs.	

Table VII. (Cont)

b) Arrays of Variables used in TFAN

DA	= $D_a$	Open loop denominator polynomial <sup>6</sup>
N32	= $N_{32}$	Numerator polynomial <sup>6</sup> of $\partial N_1 / \partial A_J$ transfer function
N43	= $N_{43}$	Numerator polynomial <sup>6</sup> of $\partial W_{2.5} / \partial A_D$ transfer function
N54	= $N_{54}$	Numerator polynomial <sup>6</sup> of $\partial N_2 / \partial W_F$ transfer function
N64	= $N_{64}$	Numerator polynomial <sup>6</sup> of $\partial P_4 / \partial W_F$ transfer function
N74	= $N_{74}$	Numerator polynomial <sup>6</sup> of $\partial T_3 / \partial W_F$ transfer function
KAN1	= $K_{AN1}$	Control gains for Fan Speed Control
KAW	= $K_{AW}$	Control gains for Corrected Air Flow Control
KWN2	= $K_{WN2}$	Control gains for H. P. Rotor Speed Control
TA2	= $A_2$	Time constants of $A_J$ actuator
TA3	= $A_3$	Time constants of $A_D$ actuator
TA4	= $A_4$	Time constants of $W_F$ actuator
TB3	= $B_3$	Time constants of $N_1$ sensor
TB4	= $B_4$	Time constants of $W_{2.5}$ sensor
TB5	= $B_5$	Time constants of $N_2$ sensor
TB6	= $B_6$	Time constants of $P_4$ sensor
TB7	= $B_7$	Time constants of $T_3$ sensor

<sup>6</sup>Polynomials expressed either in terms of (1) the coefficients of the polynomial, or (2) the time constants and gain of the polynomial. See input data format for TFAN.

Table VII. (Cont)

F	Array for the input of data using DECRD	
TITLE	Title of run in alpha-numeric characters (up to 72 characters)	
PA, PB, PC, PD, PE	Arrays used for the temporary storage of the coefficients of polynomials in intermediate computations	
RA, RB, RC	Arrays used for the temporary storage of coefficients of polynomials used to compute closed-loop characteristic polynomial	
RR, CC (Complex)	Arrays used for the temporary storage of the real and complex roots of a polynomial	
HA = (A <sub>2</sub> , B <sub>3</sub> )	Array used to store time constants of actuator and sensor of Fan Speed Control Loop	
HB = (A <sub>3</sub> , B <sub>4</sub> )	Array used to store time constants of actuator and sensor of Corrected Air Flow Control Loop	
HC = (A <sub>4</sub> , B <sub>5</sub> , B <sub>6</sub> , B <sub>7</sub> )	Array used to store time constants of actuator and sensor of H. P. Rotor Speed Control Loop	
c) <u>Real *4 Variables</u>		
FLG	≠ 0 if data entered in form supplied by P&WA	
G32	Steady-state gain for $\partial N_1 / \partial A_J$ transfer function	
G43	Steady-state gain for $\partial W_{2.5} / \partial A_D$ transfer function	
G54	Steady-state gain for $\partial N_2 / \partial W_F$ transfer function	Used only if FLG ≠ 0.
G64	Steady-state gain for $\partial P_4 / \partial W_F$ transfer function	
G74	Steady-state gain for $\partial T_3 / \partial W_F$ transfer function	
KN1 = K <sub>N1</sub>	Integrator gain for Fan Speed Control Loop	



Table VII. (Cont)

KW	= $K_{W1}$	Integrator gain for Corrected Air Flow Control Loop	
KN2	= $K_{N2}$	Integrator gain for H. P. Rotor Control Loop	
P4	= $(P_4)_0$	Initial Steady State Value of $P_4$	
WF	= $(W_F)_0$	Initial Steady State Value of $W_F$	Used only for H. P. Rotor Speed Control
N2	= $(N_2)_0$	Initial Steady State Value of $N_2$	
T3	= $(T_3)_0$	Initial Steady State Value of $T_3$	
CPO		1.0 if coefficients of closed loop characteristic polynomial printed out.	
SF		Scale factor for roots (used as a dummy argument when calling subroutine PRTX)	
d) <u>Integer *4 Variables</u>			
NDA		Degree of open loop denominator polynomial, $D_a$	
NN32		Degree of numerator polynomial of $\partial N_1 / \partial A_J$ transfer function	
NN43		Degree of numerator polynomial of $\partial W_{2.5} / \partial A_D$ transfer function	
NN54		Degree of numerator polynomial of $\partial N_2 / \partial W_F$ transfer function	
NN64		Degree of numerator polynomial of $\partial P_4 / \partial W_F$ transfer function	
NN74		Degree of numerator polynomial of $\partial T_3 / \partial W_F$ transfer function	
NTA2		Number of time constants for $A_J$ actuator	
NTA3		Number of time constants for $A_D$ actuator	
NTA4		Number of time constants for $W_F$ actuator	
NTB3		Number of time constants for $N_1$ sensor	
NTB4		Number of time constants for $W_{2.5}$ sensor	

Table VII. (Cont)

NTB5	Number of time constants for $N_2$ sensor
NTB6	Number of time constants for $P_4$ sensor
NTB7	Number of time constants for $T_3$ sensor
NAN1	Number of control gains $K_{AN1}$ for which root locus is computed
NAW	Number of control gains $K_{AW}$ for which root locus is computed
NWN2	Number of control gains $K_{WN2}$ for which root locus is computed

The following integers are used for indexing only: I, NA, NB, NC.

The following integers are used to indicate degree of polynomials for intermediate computations:

NPA, NPB, NPC, NPD, NPE, NRA, NRB, NRC

Example: NPA indicates that the first (NPA + 1) locations of array PA are used to store coefficients of a polynomial.

The following integers are used to indicate the number of locations used in an array for intermediate computations:

NHA, NHB, NHC, NCC, NRR

Example: NHA indicates that the first (NHA) locations of array HA are being used for computation.

e) List of Logical Constants for TFAN

Logical constant is .TRUE. if the expression to the right of the colon (:) is true; .FALSE. otherwise.

Symbols: a|b means a or b; a & b means a and b.

LA:  $NAN1 > 0$  Fan Speed Control Loop closed

LAN:  $NAN1 \leq 0$  Fan Speed Control Loop open

LB:  $NAW > 0$  Corrected Air Flow Control Loop closed

LBN:  $NAW \leq 0$  Corrected Air Flow Control Loop open

Table VII. Concluded

LC:	$N_{WN2} > 0$	H. P. Rotor Speed Control Loop closed
LCN:	$N_{WN2} \leq 0$	H. P. Rotor Speed Control Loop open
LDN:	$K_{N1} = 0$	No integrator gain in Fan Speed Control Loop
LEN:	$K_W = 0$	No integrator gain in Corrected Air Flow Control Loop
LFN:	$K_{N2} = 0$	No integrator gain in H. P. Rotor Control Loop
LH:	$(LDN \ \& \ LEN \ \& \ LFN) \   \ (LAN \ \& \ LBN \ \& \ LFN) \  $ $(LBN \ \& \ LCN \ \& \ LDN) \   \ (LAN \ \& \ LCN \ \& \ LEN)$	
	If LH is true, then a free $s$ term can be factored out.	
LJN:	$[(W_F)_0 = 0] \   \ [(P_4)_0 = 0]$ No $P_4$ term in H. P. Rotor Speed Control See Equations.	
LP:	$CPO = 1$	If true, then coefficients of closed loop characteristic are also printed out.

EXAMPLE CASE USING TFAN

The example case used is for a typical turbofan engine operating at sea level, zero Mach, and military power setting. The necessary transfer function polynomials required for the H. P. Rotor Speed Control (Figure 5c) are:

$$D_a = (1 + s/1.8) (1 + s/14)$$

$$N_{54} = 0.54$$

$$N_{64} = 0.03 (1 + s/4)$$

$$N_{74} = 0.016$$

The initial conditions are:

$$(P_4)_0 = 354.7 \text{ psia}$$

$$(W_F)_0 = 5822.2 \text{ lb/hr}$$

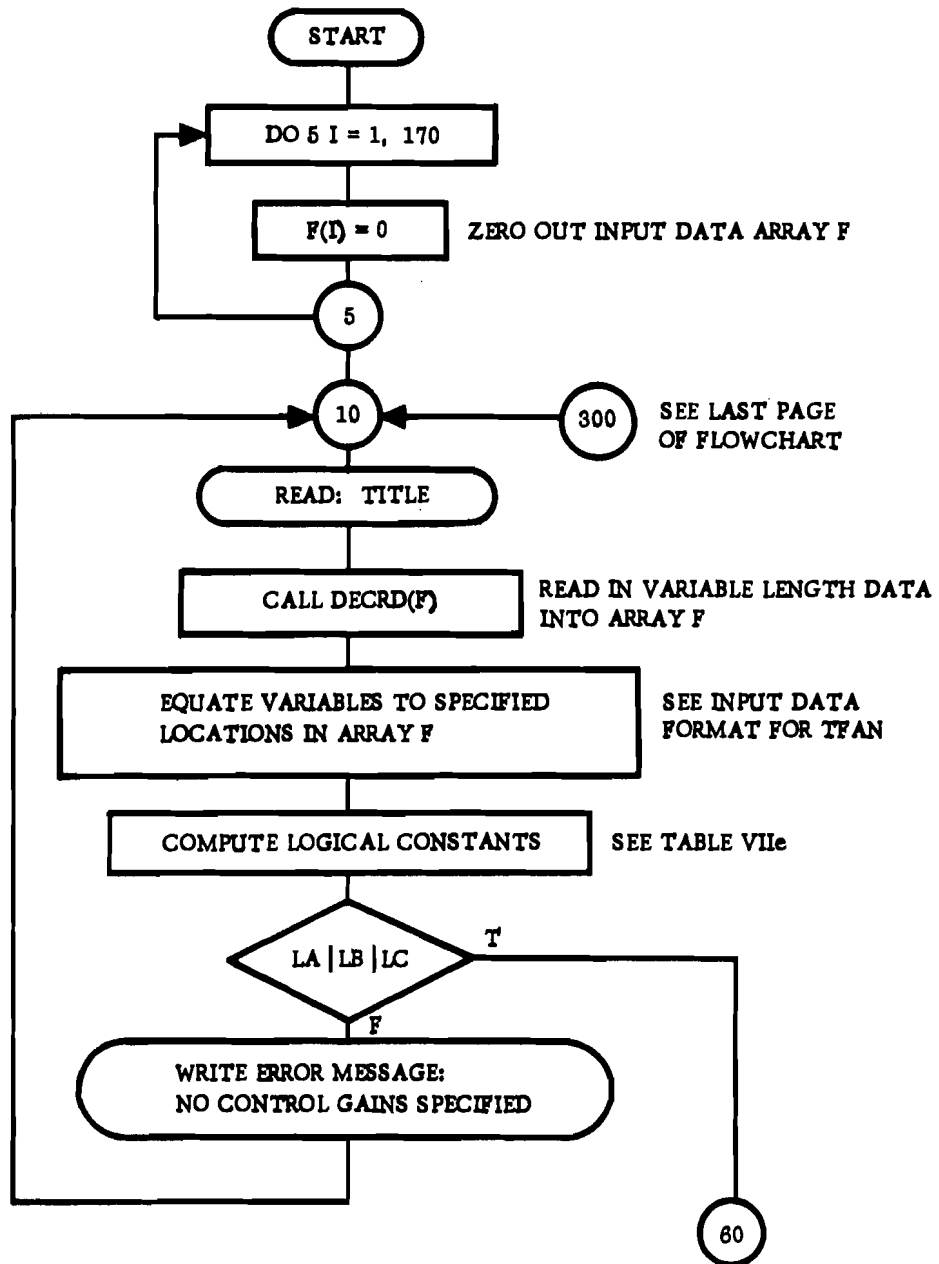


Figure 6. Flowchart of Main Program TFAN

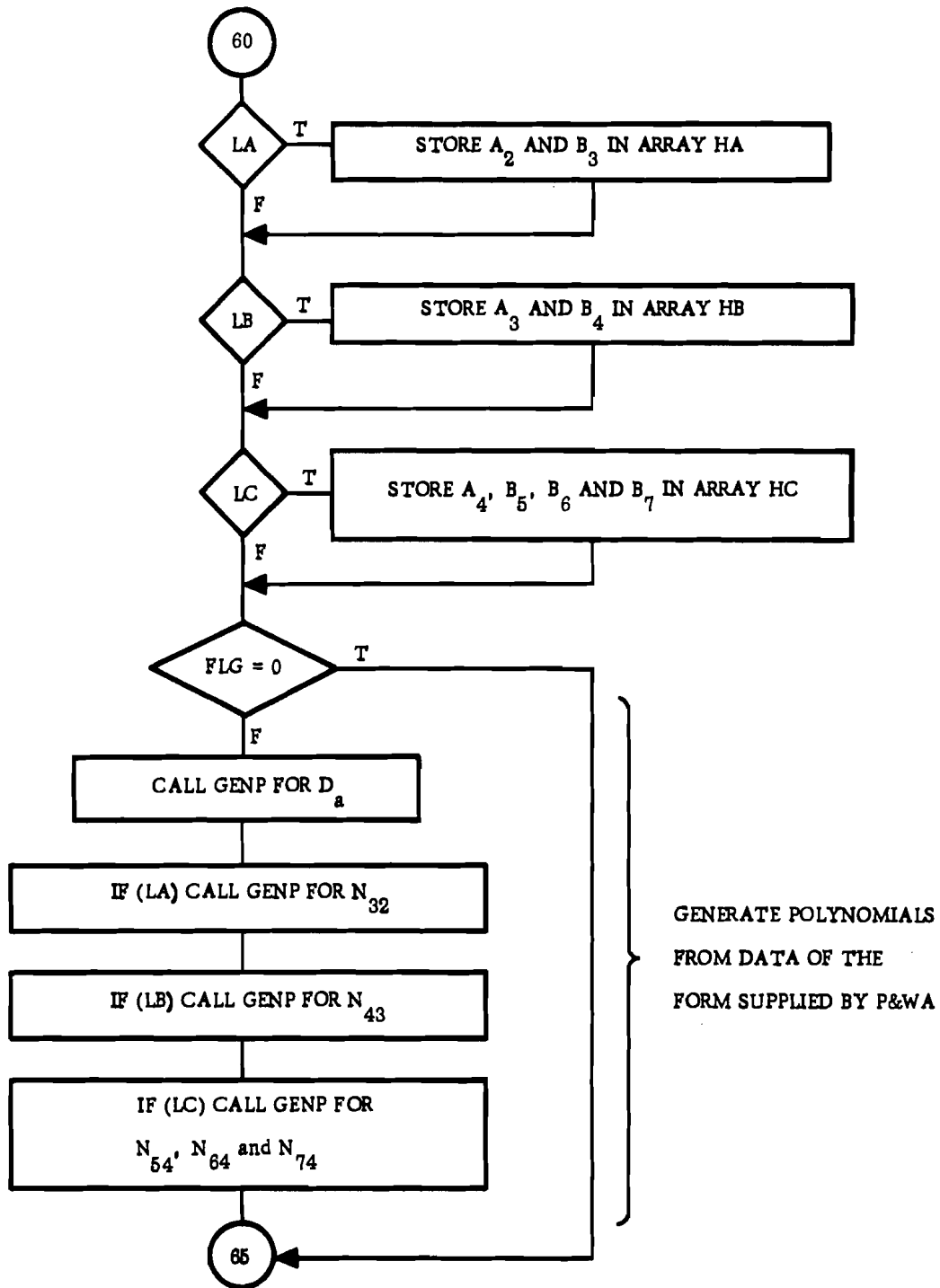


Figure 6. (Continued)

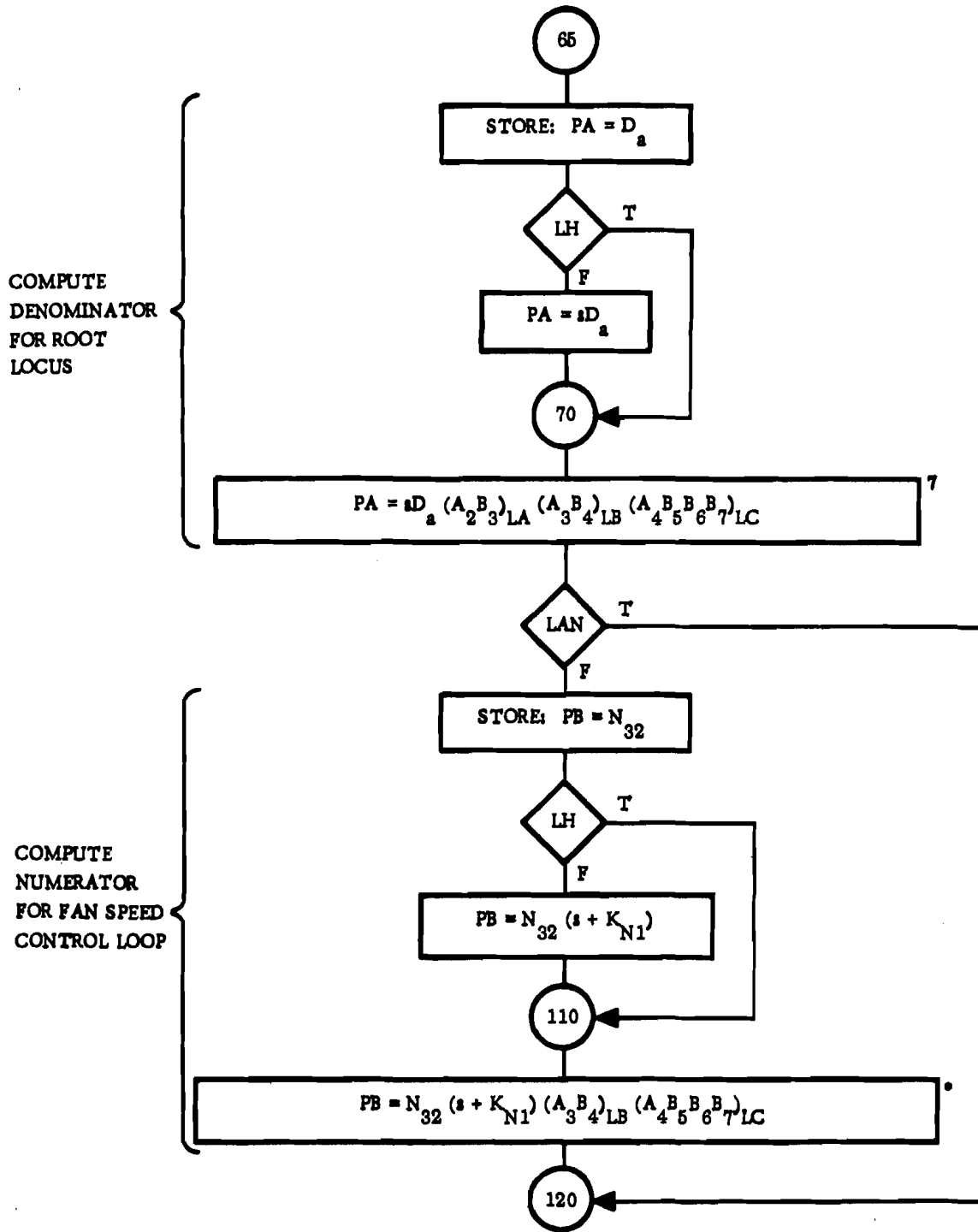


Figure 6. (Continued)

7 (A<sub>2</sub>B<sub>3</sub>)<sub>LA</sub> means (A<sub>2</sub>B<sub>3</sub>) is included in the polynomial if LA is true, etc.

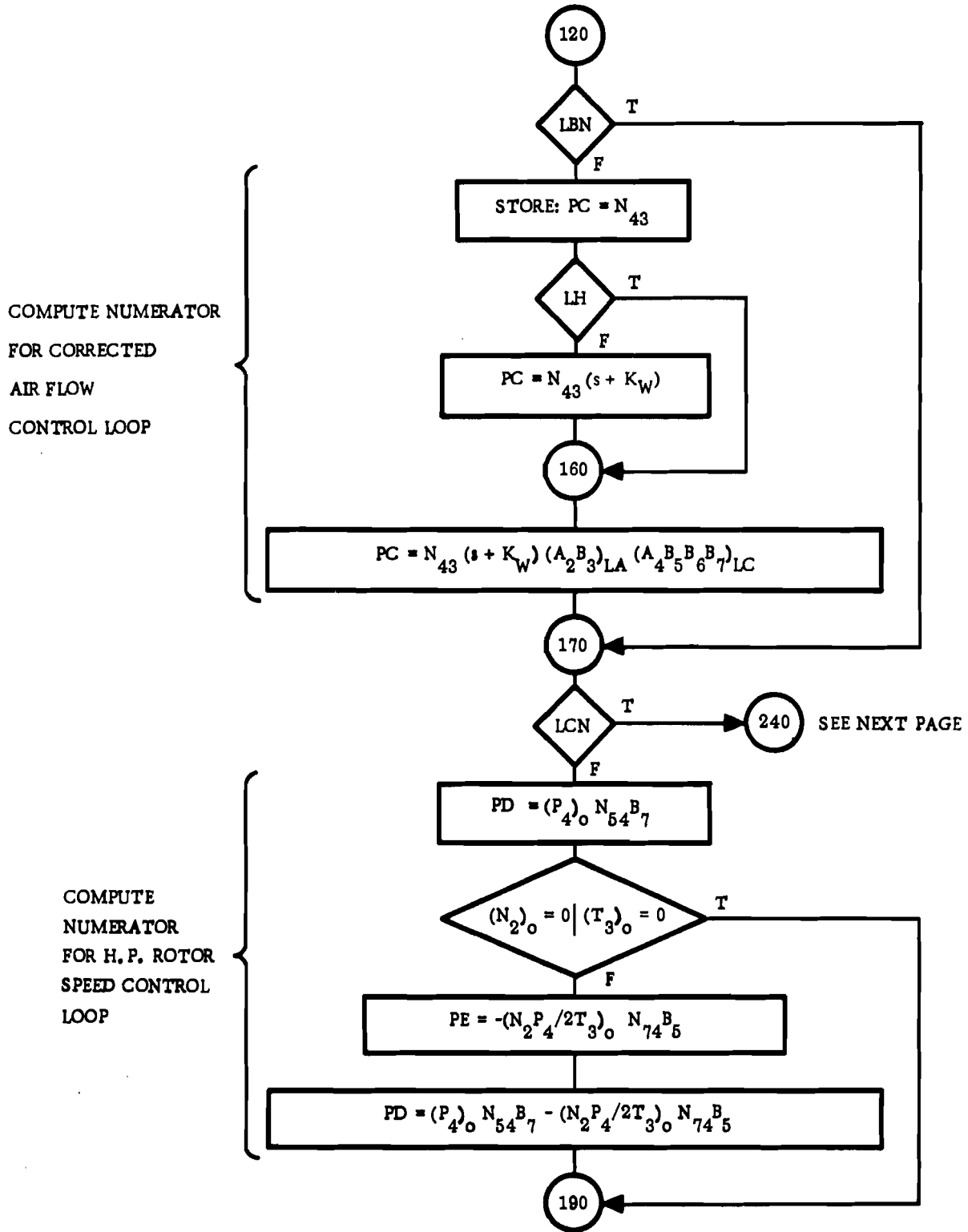


Figure 6. (Continued)

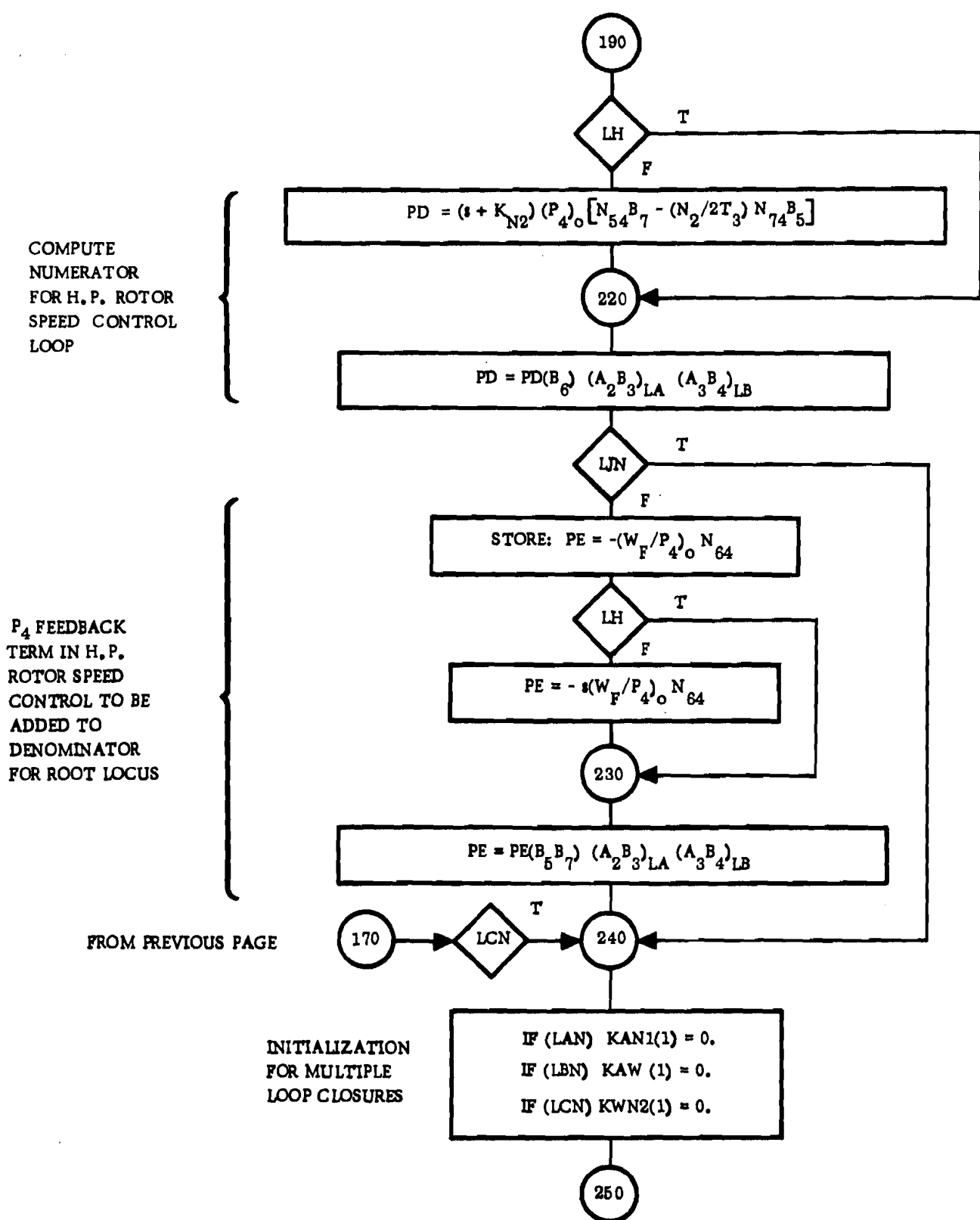


Figure 6. (Continued)



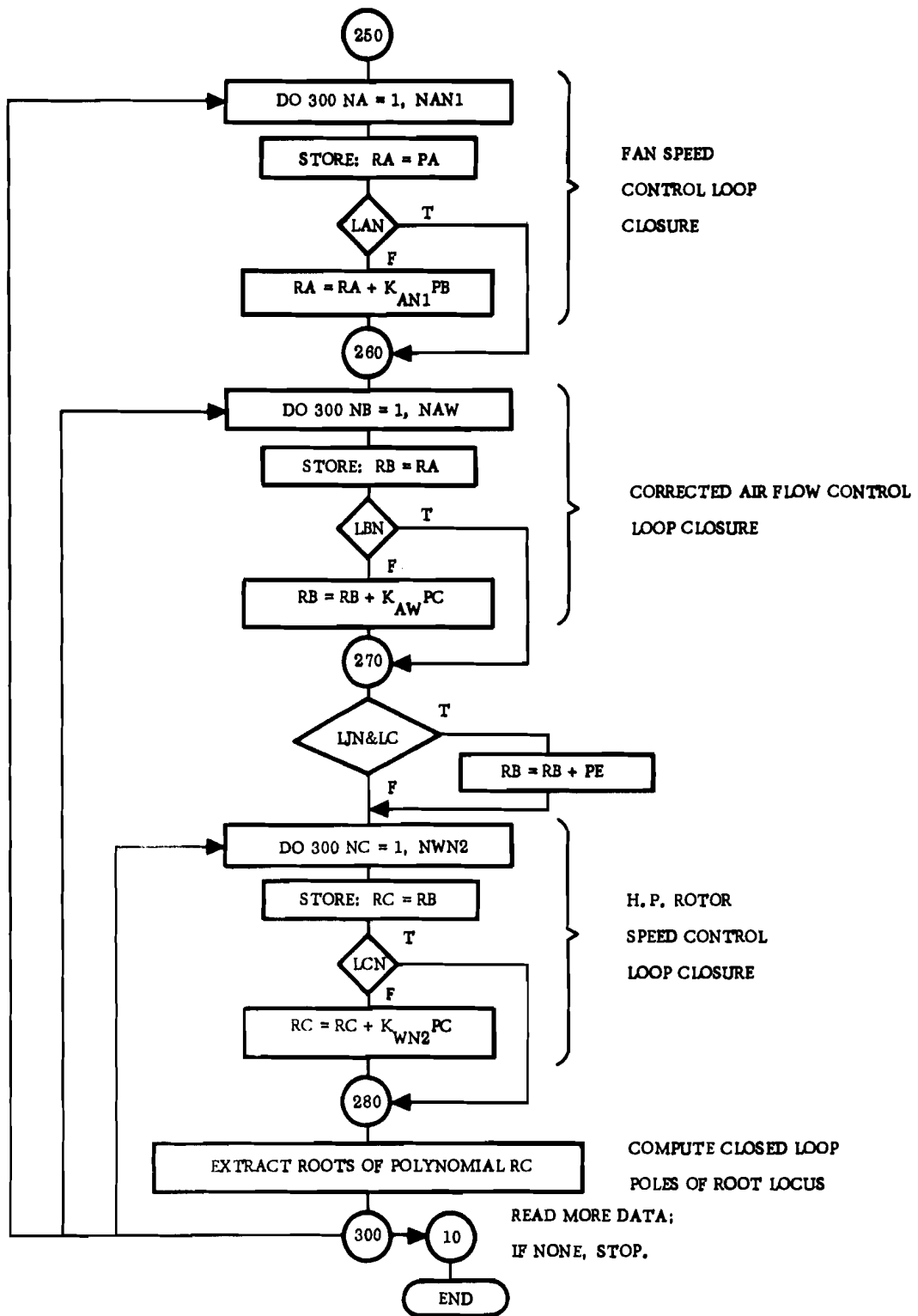


Figure 6. (Concluded)

$$(N_2)_0 = 12,800 \text{ RPM}$$

$$(T_3)_0 = 619.42 \text{ }^\circ\text{R}$$

The integrator gain is set at  $K_{N2} = 1.0 \text{ sec}^{-1}$ .

Control gains for the other control loops are set to zero, i. e.,

$$K_{AN1} = K_{AW} = 0.$$

The actuator and sensor lags are:

$$A_4 = 0.02 (s + 50)$$

$$B_5 = 0.05 (s + 20)$$

$$B_6 = 0.02 (s + 50)$$

$$B_7 = (s + 1)$$

The following computer print-out (Table X) shows the computation of the root locus for the H. P. Rotor Speed Control, for control gain  $K_{WN2}$  varying from 0. to 0.5. A plot of the root locus for this case is shown on Figure 7.

Table VIII. Fortran H Program Listing of TFAN

C	MAIN PROGRAM	00000030
C	ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR TURBOFAN ENGINE	00000040
C	E.L.LUM, FEBRUARY 1968	00000050
C		00000060
	IMPLICIT LOGICAL*4(L)	00000070
	COMPLEX*8 CC(10)	00000080
	REAL*4 DA(8),N32(8),N43(8),N54(8),N64(8),N74(8)	00000090
	REAL*4 KAN1(19),KAW(19),KWN2(19),KN1,KW,KN2,N2,TITLE(18),F(170)	00000100
	REAL*4 TA2(4),TA3(4),TA4(4),TB3(4),TB4(4),TB5(4),TB6(4),TB7(4)	00000110
	REAL*4 PA(20),PB(20),PC(20),PD(20),PE(20)	00000120
	REAL*4 RA(20),RB(20),RC(20),HA(8),HB(8),HC(16),RR(20)	00000130
	COMMON /CMB/HA,HB,HC,NHA,NHB,NHC	00000150
	EQUIVALENCE (F(2),DA),(F(12),N32),(F(22),N43),(F(32),N54),	00000160
	1(F(42),N64),(F(52),N74),(F(61),P4),(F(62),WF),(F(63),N2),	00000170
	2(F(64),T3),(F(66),KN1),(F(67),KW),(F(68),KN2),(F(72),KAN1)	00000180
	3,(F(92),KAW),(F(112),KWN2),(F(132),TA2),(F(137),TA3),(F(142),TA4)	00000190
	4,(F(147),TB3),(F(152),TB4),(F(157),TB5),(F(162),TB6),(F(167),TB7)	00000200
	5,(F(10),FLG),(F(20),G32),(F(30),G43),(F(40),G54),(F(50),G64)	00000204
	6,(F(60),G74),(F(65),CPO)	00000206
	SF=1.	00000210
	LP=.TRUE.	00000220
	DO 5 I=1,170	00000224
	5 F(I)=0.	00000226
	10 READ(5,20)TITLE	00000230
	20 FORMAT(18A4)	00000240
	WRITE(6,30)TITLE	00000250
	30 FORMAT(1H1,4X,'ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR TURBOFAN	00000260
	ENGINE '//5X,18A4)	00000270
	CALL DECRD(F)	00000280
	WRITE(6,40)	00000290
	40 FORMAT(1H0,4X,'NON-ZERO INPUT DATA'//4(10X,'I',7X,'F(I)',5X))	00000300
	CALL PRIN(F,170)	00000310
	NDA=F(1)	00000320
	NN32=F(11)	00000330
	NN43=F(21)	00000340
	NN54=F(31)	00000350
	NN64=F(41)	00000360
	NN74=F(51)	00000370

Table VIII. (Continued)

NAN1=F(71)	00000380
NAW=F(91)	00000390
NWN2=F(111)	00000400
NTA2=F(131)	00000410
NTA3=F(136)	00000420
NTA4=F(141)	00000430
NTB3=F(146)	00000440
NTB4=F(151)	00000450
NTB5=F(156)	00000460
NTB6=F(161)	00000470
NTB7=F(166)	00000480
RA(1)=1.	00000490
LA=NAN1.GT.0	00000500
LAN=.NOT.LA	00000510
LB=NAW.GT.0	00000520
LBN=.NOT.LB	00000530
LC=NWN2.GT.0	00000540
LCN=.NOT.LC	00000550
LDN=KN1.EQ.0.	00000560
LEN=KN.EQ.0.	00000570
LFN=KN2.EQ.0.	00000580
LH=LDN.AND.LEN.AND.LFN.OR.LAN.AND.LBN.AND.LFN.OR.LBN.AND.LCN.AND.	00000590
ILDN.OR.LAN.AND.LCN.AND.LEN	00000600
LJN=WF.EQ.0..OR.P4.EQ.0.	00000610
IF(LA.OR.LB.OR.LC)GO TO 60	00000620
WRITE(6,50)	00000630
50 FORMAT(IH0,4X,'OPEN LOOP, NO CONTROL GAINS SPECIFIED')	00000640
GO TO 10	00000650
60 IF(LA)CALL STREAL(TA2,NTA2,TB3,NTB3,HA,NHA)	00000660
IF(LB)CALL STREAL(TA3,NTA3,TB4,NTB4,HB,NHB)	00000670
IF(LC)CALL STREAL(TA4,NTA4,TB5,NTB5,HC,NHC)	00000680
IF(LC)CALL STR3(HC,NHC,TB6,NTB6,TB7,NTB7,HC,NHC)	00000690
IF(FLG.EQ.0.)GO TO 65	00000692
WRITE(6,62)	00000694
62 FORMAT(IH0,2X,'OPEN LOOP TRANSFER FUNCTION POLYNOMIALS GENERATED')	00000696
CALL GENP(DA,NDA,1.,'DA(S) ',2)	00000698
IF(LA)CALL GENP(NB2,NNB2,G32,'N32(S) ',2)	00000700
IF(LB)CALL GENP(NB3,NNB3,G43,'N43(S) ',2)	00000702

Table VIII. (Continued)

	IF(LC)CALL GENP(N54,NN54,G54,'N54(S) ',2)	00000704
	IF(LC)CALL GENP(N64,NN64,G64,'N64(S) ',2)	00000706
	IF(LC)CALL GENP(N74,NN74,G74,'N74(S) ',2)	00000708
C	COMPUTE DENOMINATOR, PA(S)	00000714
65	CALL GPOL(DA,NDA,1.,PA,NPA)	00000716
	IF(LH)GO TO 70	00000720
	NPA=NPA+1	00000730
	PA(NPA+1)=0.	00000740
70	CALL XPNP3(PA,NPA,LA,LB,LC,'OPEN LOOP DENOMINATOR, PA(S)',7, 1,'OPEN LOOP POLES ',4,&10)	00000750
	IF(LAN)GO TO 120	00000770
	WRITE(6,80)	00000780
80	FORMAT(1H0,2X,'FAN SPEED CONTROL LOOP CLOSED')	00000790
	CALL GPOL(N32,NN32,1.,PB,NPB)	00000800
	IF(LDN)WRITE(6,90)	00000810
90	FORMAT(1H0,4X,'NO INTEGRATOR IN FAN SPEED LOOP')	00000820
	IF(LH)GO TO 110	00000830
	WRITE(6,100)KN1	00000840
100	FORMAT(1H0,4X,'INTEGRATOR GAIN, KN1=',G12.5)	00000850
	RA(2)=KN1	00000860
	CALL POLYX(PB,NPB,RA,1,PB,NPB)	00000870
110	CALL XPNP3(PB,NPB,LAN,LB,LC,'NUMERATOR ASSOCIATED WITH KAN1, PB(S) 1 ',10,'ZEROS ASSOCIATED WITH KAN1 ',7,&10)	00000880
	120 IF(LBN)GO TO 170	00000890
	WRITE(6,130)	00000900
130	FORMAT(1H0,2X,'CORRECTED AIR FLOW CONTROL LOOP CLOSED')	00000910
	CALL GPOL(N43,NN43,1.,PC,NPC)	00000920
	IF(LFN)WRITE(6,140)	00000930
140	FORMAT(1H0,4X,'NO INTEGRATOR IN CORRECTED AIR FLOW LOOP')	00000940
	IF(LH)GO TO 160	00000950
	WRITE(6,150)KW	00000960
150	FORMAT(1H0,4X,'INTEGRATOR GAIN, KW=',G12.5)	00000970
	RA(2)=KW	00000980
	CALL POLYX(PC,NPC,RA,1,PC,NPC)	00000990
160	CALL XPNP3(PC,NPC,LA,LBN,LC,'NUMERATOR ASSOCIATED WITH KAW, PC(S) 1,9,'ZEROS ASSOCIATED WITH KAW ',7,&10)	00001000
	170 IF(LCN)GO TO 240	00001010
	WRITE(6,180)	00001020
		00001030
		00001040

Table VIII. (Continued)

180	FORMAT(1H0,2X,'H. P. ROTOR SPEED CONTROL LOOP CLOSED')	00001050
	CALL GPOL(N54,NN54,P4,PD,NPD)	00001060
	CALL XPNTAU(TB7,NTB7,PD,NPD,NPD)	00001070
	IF(N2.EQ.0..OR.T3.EQ.0.)GO TO 190	00001080
	CALL GPOL(N74,NN74,-N2/2.*P4/T3,PE,NPE)	00001090
	CALL XPNTAU(TB5,NTB5,PE,NPE,NPE)	00001094
	CALL POLADD(PD,NPD,1.,PE,NPE,1.,PD,NPD)	00001096
190	IF(LFN)WRITE(6,200)	00001100
200	FORMAT(1H0,4X,'NO INTEGRATOR IN H. P. ROTOR SPEED LOOP')	00001110
	IF(LH)GO TO 220	00001120
	WRITE(6,210)KN2	00001130
210	FORMAT(1H0,4X,'INTEGRATOR GAIN, KN2=',G12.5)	00001140
	RA(2)=KN2	00001150
	CALL POLYX(PD,NPD,RA,1,PD,NPD)	00001160
220	CALL XPNTAU(TB6,NTB6,PD,NPD,NPD)	00001170
	CALL XPNP3(PD,NPD,LA,LB,LCN,'NUMERATOR ASSOCIATED WITH KWN2, PD(S)	00001180
	1 ,10,'ZEROS ASSOCIATED WITH KWN2 ',7,&10)	00001190
	IF(LJN)GO TO 240	00001200
	CALL GPOL(N64,NN64,-WF/P4,PE,NPE)	00001210
	IF(LH)GO TO 230	00001220
	NPE=NPE+1	00001230
	PE(NPE+1)=0.	00001240
230	CALL STREAL(TB5,NTB5,TB7,NTB7,RA,NRA)	00001250
	CALL XPNTAU(RA,NRA,PE,NPE,NPE)	00001260
	CALL XPNP3(PE,NPE,LA,LB,LCN,'NUMERATOR ASSOCIATED WITH P4, PE(S)	00001270
	1,9,'ZEROS ASSOCIATED WITH P4',6,&10)	00001280
C	MULTIPLE LOOP CLOSURES	00001290
240	IF(LAN)KAN1(1)=0.	00001300
	IF(LBN)KAN(1)=0.	00001310
	IF(LCN)KWN2(1)=0.	00001320
	LP=CPO.EQ.1.	00001325
	WRITE(6,250)TITLE	00001330
250	FORMAT(1H1,4X,18A4//5X,'BEGIN LOOP CLOSURES')	00001340
	DO 300 NA=1,NANI	00001360
	CALL GPOL(PA,NPA,1.,RA,NRA)	00001365
	IF(LAN)GO TO 260	00001370
	CALL POLADD(PB,NPB,KAN1(NA),RA,NRA,1.,RA,NRA)	00001380
260	DO 300 NB=1,NAW	00001390

Table VIII. (Concluded)

CALL GPOL(RA,NRA,1.,RB,NRB)	00001400
IF(LBN)GO TO 270	00001410
CALL POLADD(PC,NPC,KAW(NB),RB,NRB,1.,RB,NRB)	00001420
270 IF(.NOT.LJN.AND.LC)CALL POLADD(PE,NPE,1.,RB,NRB,1.,RB,NRB)	00001430
DO 300 NC=1,NWN2	00001440
CALL GPOL(RB,NRB,1.,RC,NRC)	00001450
IF(LCN)GO TO 280	00001460
CALL POLADD(PD,NPD,KWN2(NC),RC,NRC,1.,RC,NRC)	00001470
280 WRITE(6,290)KAN1(NA),KAW(NB),KWN2(NC)	00001480
290 FORMAT(1H0//2X,'CONTROL GAINS: KAN1=',G12.5,', KAW=',G12.5,', KWN2	00001490
1=',G12.5)	00001500
IF(LP)CALL WRTPOL(RC,NRC,'CLOSED LOOP DENOMINATOR ',6)	00001510
CALL PRTX (RC,NRC,RR,NRR,CC,NCC,50,1.E6,SF,&10)	00001520
300 CALL WRT(RR,NRR,CC,NCC,'CLOSED LOOP POLES ',5)	00001525
WRITE(6,310)	00001530
310 FORMAT(1H0,4X,'END OF LOOP CLOSURES')	00001540
GO TO 10	00001550
END	00001560

Table IX. Input Data Format for TFAN

DECK NO. DATA PROGRAMMER E. L. LUM DATE 6-29-68 PAGE 1 of 5 JOB NO.

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1		Must be first card of run
13		
25		
37		
49		
61		
	73	80
	identification	Relative data field location in array F of main program TFAM
	1	
13	NDA	1 Degree of open-loop denominator, $D_n(s)$
25	DA(1)	2 Open-loop denominator polynomial, $D_n(s)$
37		See special instructions on previous page.
49	DA(8)	9
61	FLG	10 See special instructions on previous page.
	1 1	
13	NN32	11 Degree of numerator, $N_{32}(s)$
25	N32(1)	12 Numerator polynomial $N_{32}(s) = \partial N_1 / \Delta_f$
37		for Fan Speed Control
49	N32(8)	19 See special instructions on previous page.
61	G32	20 Gain of $N_{32}(s)$ , used only if $FLG \neq 0$
	2 1	
13	NN43	21 Degree of numerator, $N_{43}(s)$
25	N43(1)	22 Numerator polynomial $N_{43}(s) = \partial W_{2,5} / \partial A_D$
37		for Corrected Air Flow Control.
49	N43(8)	29 See special instructions on previous page.
61	G43	30 Gain of $N_{43}(s)$ , used only if $FLG \neq 0$ .

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Table IX. (Cont)

DECK NO. DATA PROGRAMMER E. L. LUM DATE 6-20-68 PAGE 3 of 8 JOB NO.

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
	3 1		
N364		31	Degree of numerator, $N_{34}(s)$
N34(1)		32	Numerator polynomial, $N_{34}(s) = \delta W_3 / W_Y$ for H. P. Rotor Speed Control
N34(0)		33	See special instructions
G34		40	Gain of $N_{34}(s)$ , used only if $FLG=0$ .
	4 1		
N404		41	Degree of numerator, $N_{44}(s)$
N44(1)		42	Numerator polynomial, $N_{44}(s) = \delta P / \delta W_Y$
N44(0)		43	See special instructions
G44		50	Gain of $N_{44}(s)$ , used only if $FLG=0$
	5 1		
N74		51	Degree of numerator, $N_{74}(s)$
N74(1)		52	Numerator polynomial, $N_{74}(s) = \delta T_3 / \delta W_Y$ for H. P. Rotor Speed Control
N74(0)		53	See special instructions
G74		60	Gain of $N_{74}(s)$ , used only if $FLG=0$
	6 1		
P4		61	$(P_4)_0$ initial steady-state value of $P_4$
WY		62	$(W_Y)_0$ " " " " " $W_Y$ For H. P.
N2		63	$(N_2)_0$ " " " " " $N_2$ Rotor Speed
T3		64	$(T_3)_0$ " " " " " $T_3$ Control Only
CPO		65	Check-out print option, 1. if print-out desired

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Table IX. (Cont)

DECK NO. DATA PROGRAMMER E. L. LUM DATE 6-28-68 PAGE 3 of 5 JOB NO.

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
6 6		
KNI		66 Integrator gain $K_{NI}$ for Fm Speed Control
KW		67 Integrator gain $K_W$ for Corrected Air Flow Control
KNS		68 Integrator gain $K_{NS}$ for H. P. Rotor Speed Control
Not Used	73	69
Not Used		70
7 1		
NANI		71 No. of control gain, $K_{ANI}$ ; 0. if Fm Speed Loop open
KANI(1)		72 } Set of control gains $K_{ANI}$ for which closed-loop
		characteristic is computed for Fm Speed
		Control Loop.
KANI(19)	73	90
9 1		
NAW		91 No. of control gains, $K_{AW}$ ; 0. if Corrected Air Flow Loop open
KAW(1)		92 } Set of control gains $K_{AW}$ for which closed loop
		characteristic is computed for Corrected
		Air Flow Control Loop.
KAW(19)	74	110
1 1 1		
NWNS		111 No. of control gains, $K_{WNS}$ ; 0. if H. P. Rotor Speed Loop open
KWNS(1)		112 } Set of control gains $K_{WNS}$ for which closed-loop
		characteristic is computed for H. P. Rotor
		Speed Control Loop.
KWNS(19)	75	130

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Table IX. (Cont)

DECK NO. DATA PROGRAMMER E. L. LUM DATE 6-30-68 PAGE 4 of 5 JOB NO.

	NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	1 3 1		
13	NTA2		131 No. of time constants for $A_2$
25	TA2(1)		132 } 133 Set of time constants for
37			
49		73 80	134 $A_2$ actuator 1/A2 for Fan Speed Control.
61	TA2(4)		135 }
1	1 3 6		
13	NTA3		136 No. of time constants for $A_3$
25	TA3(1)		137 } 138 Set of time constants for
37			
49		73 80	139 $A_D$ actuator 1/A <sub>3</sub> for Corrected Air Flow Control
61	TA3(4)		140 }
1	1 4 1		
13	NTA4		141 No. of time constants for $A_4$
25	TAM(1)		142 } 143 Set of time constants for
37			
49		73 80	144 $W_F$ actuator 1/A <sub>4</sub> for H. P. Rotor Speed Control
61	TAM(4)		145 }
1	1 4 6		
13	NTB3		146 No. of time constants for $B_3$
25	TB3(1)		147 } 148 Set of time constants for $N_1$ Sensor 1/B <sub>3</sub>
37			
49		73 80	149 for Fan Speed Control
61	TB3(4)		150 }

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Table IX. (Concluded)

DECK NO. DATA PROGRAMMER E. L. LUM DATE 6-30-68 PAGE 5 of 5 JOB NO.

	NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1			
13	1 5 1		
25	NTB4		151 No. of time constants for B <sub>4</sub>
37	TB4(1)		152
49			153 Set of time constants for W <sub>2-3</sub> sensor 1/B <sub>4</sub>
61	TB4(4)		154 for Corrected Air Flow Control
			155
1			
13	1 5 6		
25	NTB5		156 No. of time constants for B <sub>5</sub>
37	TB5(1)		157
49			158 Set of time constants for N <sub>2</sub> sensor 1/B <sub>5</sub>
61	TB5(4)		159 for H. P. Rotor Speed Control
			160
1			
13	1 6 1		
25	NTB6		161 No. of time constants for B <sub>6</sub>
37	TB6(1)		162
49			163 Set of time constants for P <sub>4</sub> sensor 1/B <sub>6</sub>
61	TB6(4)		164 for H. P. Rotor Speed Control
			165
1			
13	1 6 6		Minus sign must be on last card of run.
25	NTB7		166 No. of time constants for B <sub>7</sub>
37	TB7(1)		167
49			168 Set of time constants for T <sub>2</sub> sensor 1/B <sub>7</sub>
61	TB7(4)		169 for H. P. Rotor Speed Control
			170

Table X. Computer Printout for Example Case Using TFAN

ROOT LOCUS FOR MULTIPLE LOOP CLOSURES FOR TURBOFAN ENGINE

EXAMPLE CASE USING TFAN, H.P. ROTOR SPEED CONTROL

NON-ZERO INPUT DATA (SEE FORMAT OF INPUT DATA)

I	F(I)	I	F(I)	I	F(I)	I	F(I)
1	2.00000	2	1.80000	3	14.0000	10	1.00000
40	0.540000	41	1.00000	42	4.00000	50	0.300000E-01
60	0.160000E-01	61	352.700	62	5822.20	63	12800.0
64	619.420	65	1.00000	68	1.00000	111	14.0000
113	0.100000E-02	114	0.200000E-02	115	0.300000E-02	116	0.500000E-02
117	0.100000E-01	118	0.200000E-01	119	0.300000E-01	120	0.500000E-01
121	0.700000E-01	122	0.100000E 00	123	0.200000	124	0.300000
125	0.500000	141	1.00000	142	0.200000E-01	156	1.00000
157	0.500000E-01	161	1.00000	162	0.200000E-01	166	1.00000
167	1.00000						

OPEN LOOP TRANSFER FUNCTION POLYNOMIALS GENERATED

DA(S)

POLYNOMIAL OF ORDER 2, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.3968253E-01    0.6269843    1.000000

N54(S)

POLYNOMIAL OF ORDER 0, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.5400000

N64(S)

POLYNOMIAL OF ORDER 1, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.7499997E-02    0.3000000E-01

N74(S)

POLYNOMIAL OF ORDER 0, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.1600000E-01

Polynomials generated  
by subroutine GENP

OPEN LOOP DENOMINATOR, PA(S)

POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.7936504E-06    0.1095714E-03    0.5203962E-02    0.1036072    0.8154953  
 1.716984    1.000000    0.0

Compute  
open-loop  
denominator

OPEN LOOP POLES

NUMBER OF REAL ROOTS= 7  
 -1.799993    -1.000002    -19.99992    -14.00016    -49.99997

Table X. (Continued)

-49.95986	0.0			
H.P. ROTOR SPEED CONTROL LOOP CLOSED				
<del>INTEGRATOR GAIN, KN2= 1.0000</del>				
NUMERATOR ASSOCIATED WITH K <sub>N2</sub> , PD(S)				
POLYNOMIAL OF ORDER 3, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE				
3.750852	193.9365	322.3364	132.1510	} Compute numerator for root locus
<del>ZEROS ASSOCIATED WITH K<sub>N2</sub></del>				
NUMBER OF REAL ROOTS= 3				
-0.9999949	-0.7046493	-50.00000		
<del>NUMERATOR ASSOCIATED WITH P<sub>4</sub>, PE(S)</del>				
POLYNOMIAL OF ORDER 4, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE				
-0.6190311E-02	-0.1547577	-0.6437926	-0.4952251	0.0
<del>ZEROS ASSOCIATED WITH P<sub>4</sub></del>				
NUMBER OF REAL ROOTS= 4				
-4.000005	-1.000000	-19.99997	0.0	} P <sub>4</sub> term to be added to open- loop denominator

Table X. (Continued)

EXAMPLE CASE USING TFAN, H.P. ROTOR SPEED CONTROL

BEGIN LOOP CLOSURES

CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.0

These gains are set to zero.

Variable gain

---

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	0.6607376
1.073191	0.5047749	0.0		

CLOSED LOOP POLES  
 NUMBER OF REAL ROOTS= 5  
 -1.060050      -1.000072      -19.99988      -10.32411      0.0  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 -52.20795      13.41269

Denominator for root locus, P<sup>4</sup> term added to open-loop denominator

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CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.10000E-02

---

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	0.6644884
1.267127	0.8271112	0.1321510		

CLOSED LOOP POLES  
 NUMBER OF REAL ROOTS= 5  
 -0.2333040      -1.280692      -1.000019      -9.326349      -20.56915  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 -52.19524      13.43887

First control gain change, K<sub>WN2</sub> = 0.001

CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.20000E-02

---

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	0.6682392
1.461063	1.149447	0.2643021		

CLOSED LOOP POLES

Table X. (Continued)

NUMBER OF REAL ROOTS= 5

~~-1.000001~~     ~~-0.3928037~~     ~~-8.304079~~     ~~-1.668417~~     ~~-21.06929~~  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 -52.18265     13.46566

CONTROL GAINS: KAN1= 0.0     , KAM= 0.0     , KMN2= 0.30000E-02

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06     0.1085714E-03     0.5203962E-02     0.9741688E-01     0.6719901  
 1.655000     1.471784     0.3964531

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 5  
~~-0.4867685~~     ~~-2.293941~~     ~~-1.000003~~     ~~-7.159027~~     ~~-21.52005~~  
 NUMBER OF COMPLEX PAIR ROOTS= 1  
 -52.17001     13.49223

CONTROL GAINS: KAN1= 0.0     , KAM= 0.0     , KMN2= 0.50000E-02

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06     0.1085714E-03     0.5203962E-02     0.9741688E-01     0.6794918  
 2.042872     2.116455     0.6607550

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 3  
~~-0.9999929~~     ~~-0.5159929~~     ~~-22.31532~~  
 NUMBER OF COMPLEX PAIR ROOTS= 2  
 -4.309188     1.935585     -52.14510     13.54541

CONTROL GAINS: KAN1= 0.0     , KAM= 0.0     , KMN2= 0.10000E-01

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06     0.1085714E-03     0.5203962E-02     0.9741688E-01     0.6982461  
 3.012554     3.728137     1.321509



Table X. (Continued)

CLOSED LOOP POLES  
 NUMBER OF REAL ROOTS= 3  
 -0.9999968      -0.6435101      -23.92505  
 NUMBER OF COMPLEX PAIR ROOTS= 2  
 -3.532336      4.981954      -52.08340      13.67929

CONTROL GAINS: KAN1= 0.0      , KAW= 0.0      , KWN2= 0.20000E-01

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.7936504E-06      0.1085714E-03      0.5203962E-02      0.9741688E-01      0.7357545  
 4.951920      6.951502      2.643021

CLOSED LOOP POLES  
 NUMBER OF REAL ROOTS= 3  
 -0.6751729      -0.5999958      -26.33441  
 NUMBER OF COMPLEX PAIR ROOTS= 2  
 -2.431242      7.667241      -51.96394      13.95483

CONTROL GAINS: KAN1= 0.0      , KAW= 0.0      , KWN2= 0.30000E-01

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.7936504E-06      0.1085714E-03      0.5203962E-02      0.9741688E-01      0.7732631  
 6.891284      10.17487      3.964531

CLOSED LOOP POLES  
 NUMBER OF REAL ROOTS= 3  
 -0.6852608      -0.9999967      -28.20828  
 NUMBER OF COMPLEX PAIR ROOTS= 2  
 -1.602321      9.317381      -51.85086      14.23878

CONTROL GAINS: KAN1= 0.0      , KAW= 0.0      , KWN2= 0.50000E-01

CLOSED LOOP DENOMINATOR  
 POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE  
 0.7936504E-06      0.1085714E-03      0.5203962E-02      0.9741688E-01      0.8482801  
 10.77001      16.62157      6.607552

70

Table X. (Continued)

CLOSED LOOP POLES				
NUMBER OF REAL ROOTS= 3				
-0.9999901	-0.6931489	-31.14755		
NUMBER OF COMPLEX PAIR ROOTS= 2				
-0.3313532	11.55170	-51.64830	14.82947	
CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.70000E-01				
CLOSED LOOP DENOMINATOR				
POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE				
0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	0.9232971
14.64874	23.06830	9.250572		
CLOSED LOOP POLES				
NUMBER OF REAL ROOTS= 3				
-0.9999917	-0.6964747	-33.45343		
NUMBER OF COMPLEX PAIR ROOTS= 2				
0.6600275	13.14172	-51.48506	15.44758	
CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.10000E 00				
CLOSED LOOP DENOMINATOR				
POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE				
0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	1.035822
20.46681	32.73839	13.21510		
CLOSED LOOP POLES				
NUMBER OF REAL ROOTS= 3				
-0.6989459	-0.5999989	-36.16368		
NUMBER OF COMPLEX PAIR ROOTS= 2				
1.858982	14.94720	-51.32767	16.40396	
CONTROL GAINS: KAN1= 0.0 , KAW= 0.0 , KWN2= 0.20000				
CLOSED LOOP DENOMINATOR				
POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE				
0.7936504E-06	0.1085714E-03	0.5203962E-02	0.9741688E-01	1.410908
39.86046	64.97203	26.43021		

Table X. (Concluded)

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 3

-0.9999959      -0.7018111      -41.42575

NUMBER OF COMPLEX PAIR ROOTS= 2

4.677513      18.86580      -51.51369      19.44998

CONTROL GAINS: KAN1= 0.0      , KAW= 0.0      , KWN2= 0.30000

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06      0.1085714E-03      0.5203962E-02      0.9741688E-01      1.785992

59.25410      97.20566      39.64529

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 3

-0.9999958      -0.7027591      -43.87103

NUMBER OF COMPLEX PAIR ROOTS= 2

6.661975      21.44598      -52.27505      21.91109

CONTROL GAINS: KAN1= 0.0      , KAW= 0.0      , KWN2= 0.50000

CLOSED LOOP DENOMINATOR

POLYNOMIAL OF ORDER 7, COEFFICIENTS IN DESCENDING ORDER OF VARIABLE

0.7936504E-06      0.1085714E-03      0.5203962E-02      0.9741688E-01      2.536162

98.04141      161.6730      66.07552

CLOSED LOOP POLES

NUMBER OF REAL ROOTS= 3

-0.9999953      -0.7035168      -46.07709

NUMBER OF COMPLEX PAIR ROOTS= 2

-54.07115      25.49562      9.561440      25.04567

END OF LOOP CLOSURES

IHC217I

TRACEBACK FOLLOWS ROUTINE ISN REG. 14

IBCOM 82014108

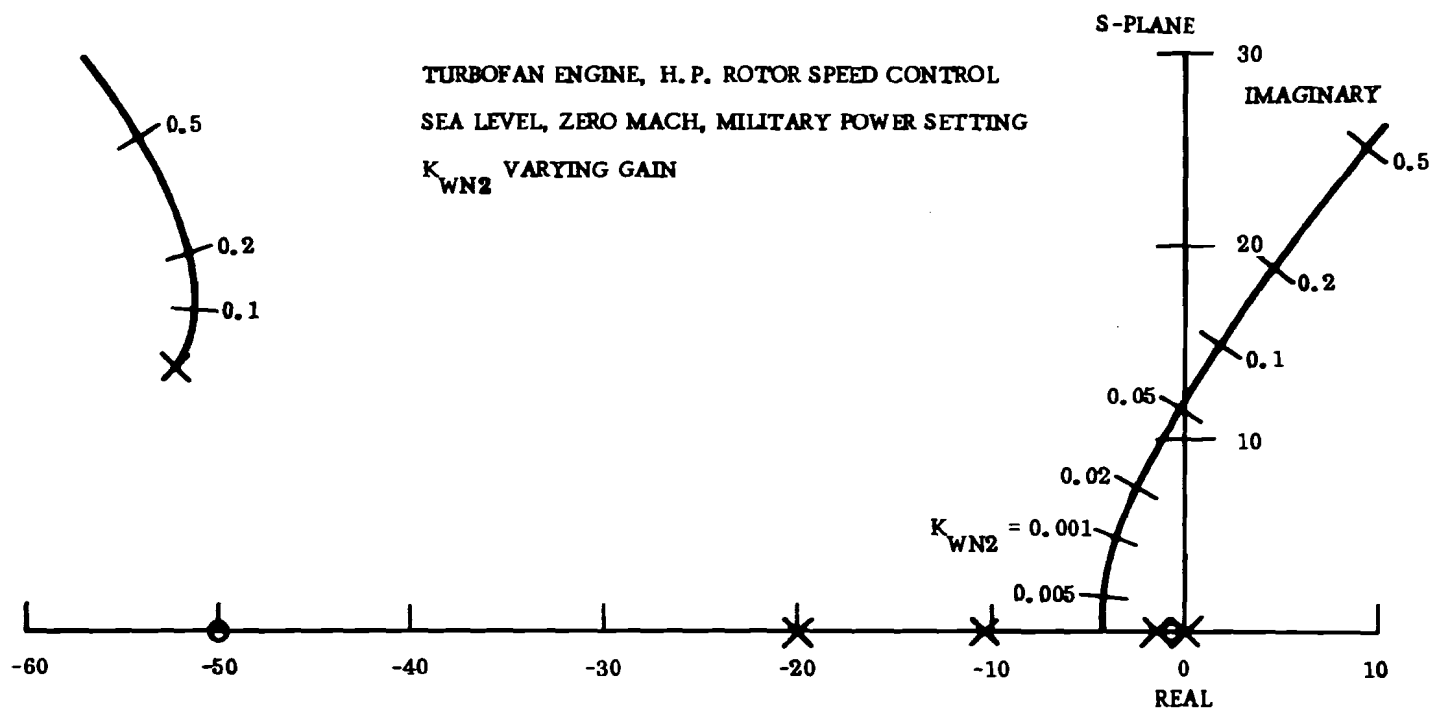


Figure 7. Root Locus for Example Case Using TFAN

#### IV. NEW COMPUTER SUBPROGRAMS DEVELOPED FOR TJET AND TFAN

The following subroutines were developed specifically for use with main programs TJET and TFAN to (1) expand polynomials with the appropriate sets of actuator or sensor lags given in terms of time constants, and (2) to facilitate handling of data of the form received from P&WA (See description of GENP). The following pages contain

1. Subroutine XPNTAU - Flowchart and program listing
2. Subroutine XPNP5 - Flowchart and program listing
3. Subroutine GENP - Flowchart and program listing

Subroutine XPNP5 is required for main program TJET only. Subroutine XPNP3 for main program TFAN only is similar to XPNP5 except that XPNP3 expands a polynomial with up to three sets of first-order lag time constants rather than five sets of time constants as in XPNP5.

#### DESCRIPTION OF SUBROUTINE XPNTAU

This subroutine is used to combine the appropriate actuator or sensor poles with the polynomials used in computing the root locus. The actuator or sensor poles are expressed as a set of first-order time constants. Subroutine XPNTAU expands a polynomial  $p_1(s)$  to the form

$$p_n(s) = p_1(s) (\tau_1 s + 1) (\tau_2 s + 1) \dots (\tau_{ntau} s + 1)$$

The flowchart for subroutine XPNTAU is shown on Figure 8, and the Fortran H program listing is shown on Table XI. The arguments for XPNTAU are:

TAU	Array of time constants, $\tau_i$ , $i = 1, 2, \dots, ntau$
NTAU	Number of time constants in array TAU
P	Coefficients of polynomial to be expanded, $p_k$ , $k = 1, \dots, np$
NPI	Initial degree of polynomial $p_1(s)$
NP	Final degree of expanded polynomial $p_n(s)$

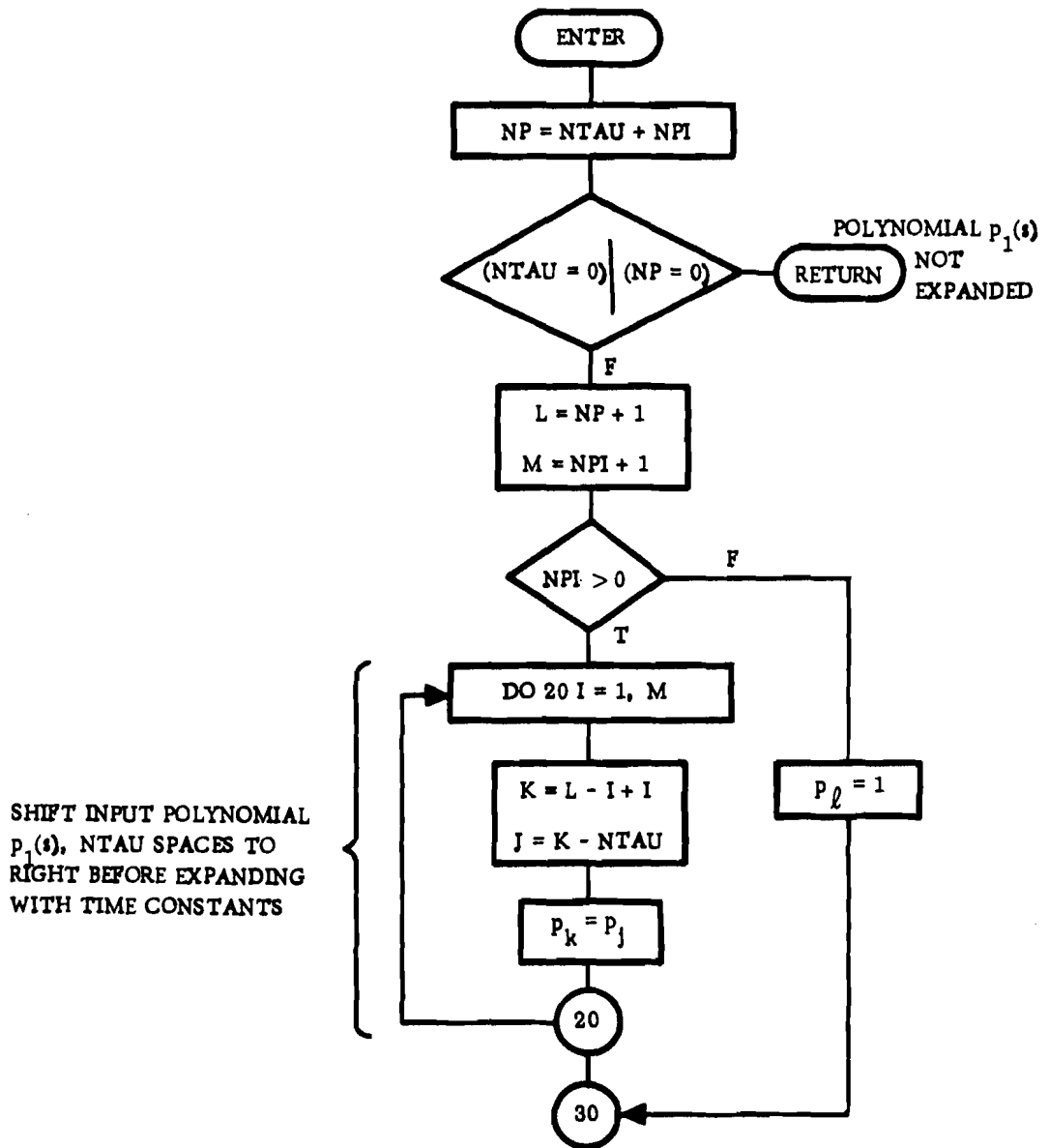


Figure 8. Flowchart for Subroutine XPNTAU

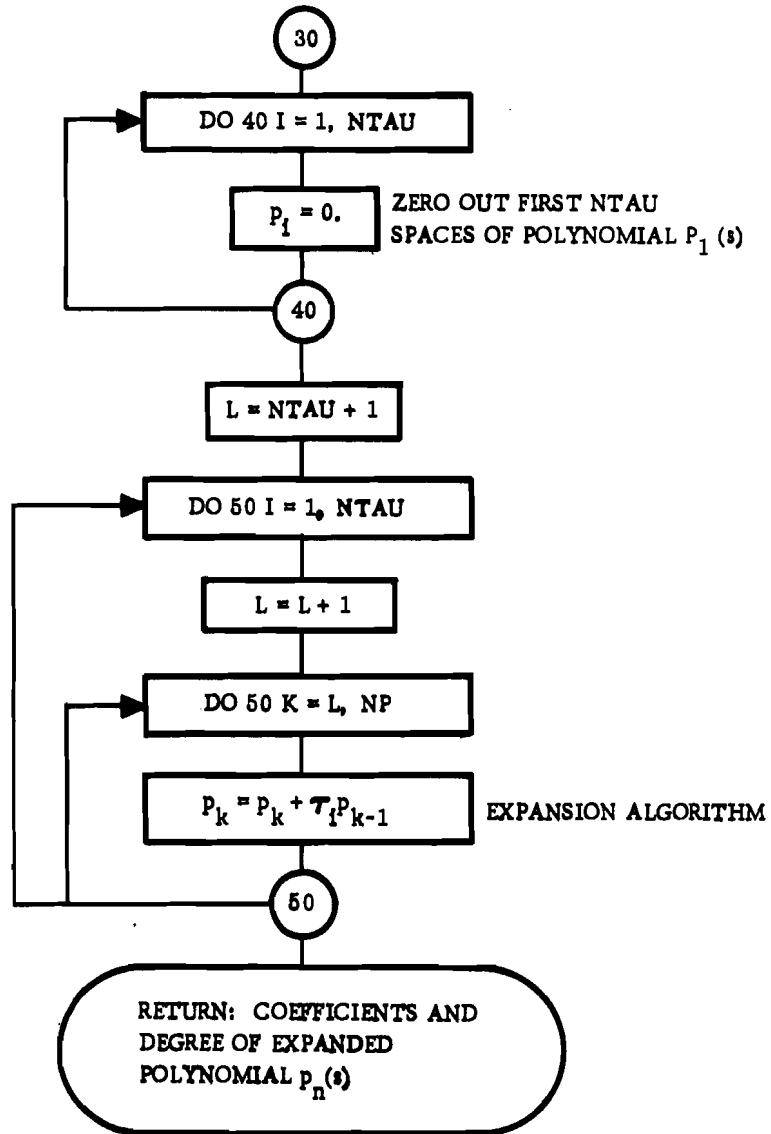


Figure 8. (Concluded)

Table XI. Fortran H Program Listing for Subroutine XPNTAU

	SUBROUTINE XPNTAU(TAU,NTAU,P,NPI,NP)	D1000010
C	THIS SUBROUTINE EXPANDS A POLYNOMIAL P(S) TO THE FORM	D1000020
C	$P(S) * (TAU(1) * S + 1) * \dots * (TAU(NTAU) * S + 1)$	D1000030
C	DEVELOPED BY E. L. LUM FEBRUARY 1968	D1000040
C		D1000050
	REAL*4 TAU(1),P(1)	D1000060
	NP=NTAU+NPI	D1000070
	IF(NTAU.EQ.0.OR.NP.EQ.0)RETURN	D1000080
	L=NP+1	D1000090
	M=NPI+1	D1000100
	DO 20 I=1,M	D1000140
	K=L-I+1	D1000150
	J=K-NTAU	D1000160
	20 P(K)=P(J)	D1000170
	DO 40 I=1,NTAU	D1000180
	40 P(I)=0.	D1000190
	L=NTAU+1	D1000200
	DO 50 I=1,NTAU	D1000210
	L=L-I	D1000220
	DO 50 K=L,NP	D1000230
	50 P(K)=P(K)+P(K+1)*TAU(I)	D1000240
	RETURN	D1000250
	END	D1000260



## DESCRIPTION OF SUBROUTINE XPNP5

This subroutine is used to combine five or less sets of actuator and sensor poles with a polynomial. The actuator and sensor poles are expressed as first-order time constants. Logical statements are used to determine which poles are to be combined with the given polynomial  $p_1(s)$ , i. e. ,

$$p_n(s) = p_1(s) (A)_{LA} (B)_{LB} (C)_{LC} (D)_{LD} (E)_{LE}$$

where  $(A)_{LA}$  means that the poles from set A are combined with  $p_1(s)$  if LA is true, etc.

The flowchart for subroutine XPNP5 is shown on Figure 9, and the Fortran H program listing is shown on Table XII. The arguments for XPNP5 are:

P	Polynomial to be expanded, $p(s)$
NP	Initial degree of polynomial $p(s)$ ; returned as final degree of $p(s)$
LA, LB, LC, LD, LE	Logical constants, if true expands polynomial $p(s)$ by first-order lags from set A, B, C, D, or E, respectively
TA	Title to be printed with expanded polynomial p
NTA	Length of title TA (Number of characters in multiples of 4)
TB	Title to be printed with extracted roots of expanded polynomial p
NTB	Length of title TB (Number of characters in multiples of 4)
*	Non-standard return in case of error in extracting roots

The variables that are passed by COMMON to simplify the programming and to save time and storage are:

A, B, C, D, E	Sets of first-order lags expressed in terms of time constants
NA, NB, NC, ND, NE	Number of first-order lags in set A, B, C, D, or E, respectively

## DESCRIPTION OF SUBROUTINE GENP

This subroutine is used to facilitate data handling by converting transfer function data of the form supplied by P&WA into coefficients of s-plane polynomials. The transfer function data are expressed in terms of the first-order lag frequencies ( $a_j$ ) and the final steady state gain ( $g$ ) of the transfer function. Subroutine GENP generates the coefficients of a polynomial of the form

$$a(s) = g(1 + s/a_1) (1 + s/a_2) \dots (1 + s/a_{na}).$$

The flowchart for subroutine GENP is shown on Figure 10, and the Fortran program listing is shown on Table XIII. The arguments used for GENP are:

- A     Array of first-order lag frequencies,  $a_i$ ,  $i=1, 2, \dots, na$ ; also array in which generated polynomial is returned,  $a(s)$
- NA    Number of first-order lags in A
- G     Steady state of expanded polynomial  $a(s)$
- T     Title to be printed with expanded polynomial  $a(s)$
- NT    Length of title T (Number of characters in multiples of 4)

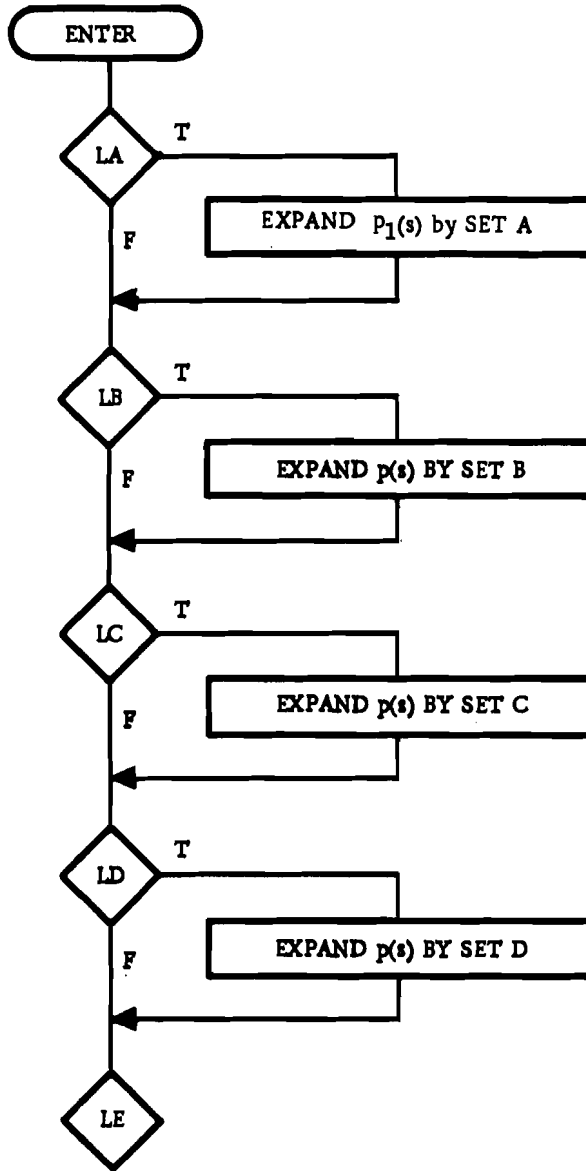


Figure 9. Flowchart for Subroutine XPNP5

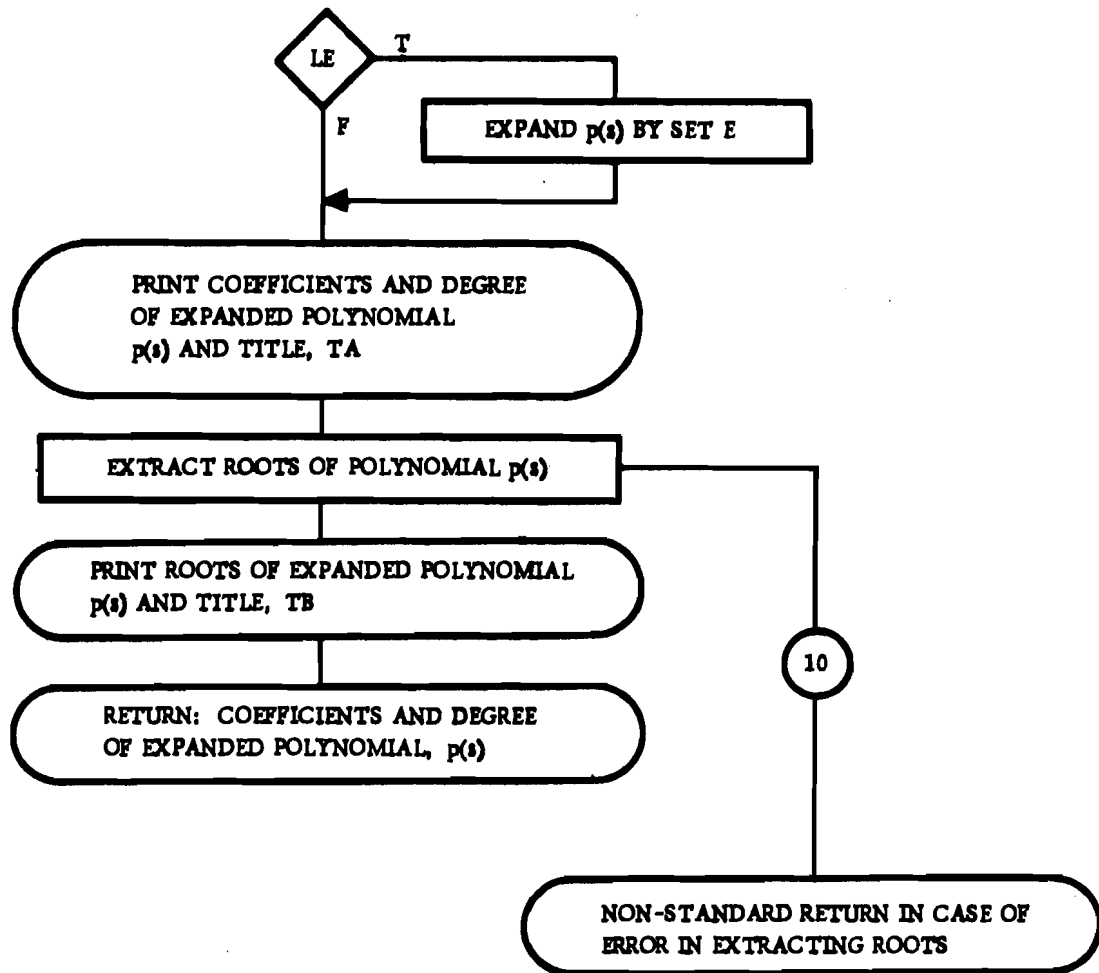


Figure 9. (Concluded)

Table XII. Fortran H Program Listing for Subroutine XPNP5

	SUBROUTINE XPNP5(P, NP, LA, LB, LC, LD, LE, TA, NTA, TB, NTB, *)	X0000010
C	THIS SUBROUTINE EXPANDS A POLYNOMIAL WITH UP TO FIVE SETS OF	X0000020
C	DYNAMIC LAGS SPECIFIED BY TIME CONSTANTS.	X0000030
C		X0000040
	LOGICAL*4 LA, LB, LC, LD, LE	X0000050
	COMPLEX*8 CC(10)	X0000060
	REAL*4 P(1), TA(1), TB(1), A(4), B(4), C(4), D(4), E(4), RR(20)	X0000070
	COMMON /CMB/A, B, C, D, E, NA, NB, NC, ND, NE	X0000090
	IF(LA)CALL XPNTAU(A, NA, P, NP, NP)	X0000100
	IF(LB)CALL XPNTAU(B, NB, P, NP, NP)	X0000110
	IF(LC)CALL XPNTAU(C, NC, P, NP, NP)	X0000120
	IF(LD)CALL XPNTAU(D, ND, P, NP, NP)	X0000130
	IF(LE)CALL XPNTAU(E, NE, P, NP, NP)	X0000140
	CALL WRTPOL(P, NP, TA, NTA)	X0000150
	CALL PRX(P, NP, RR, NRR, CC, NCC, 50, 1.E6, 1., &10)	X0000160
	CALL WRT(RR, NRR, CC, NCC, TB, NTB)	X0000165
	RETURN	X0000170
	10 RETURN 1	X0000180
	END	X0000190

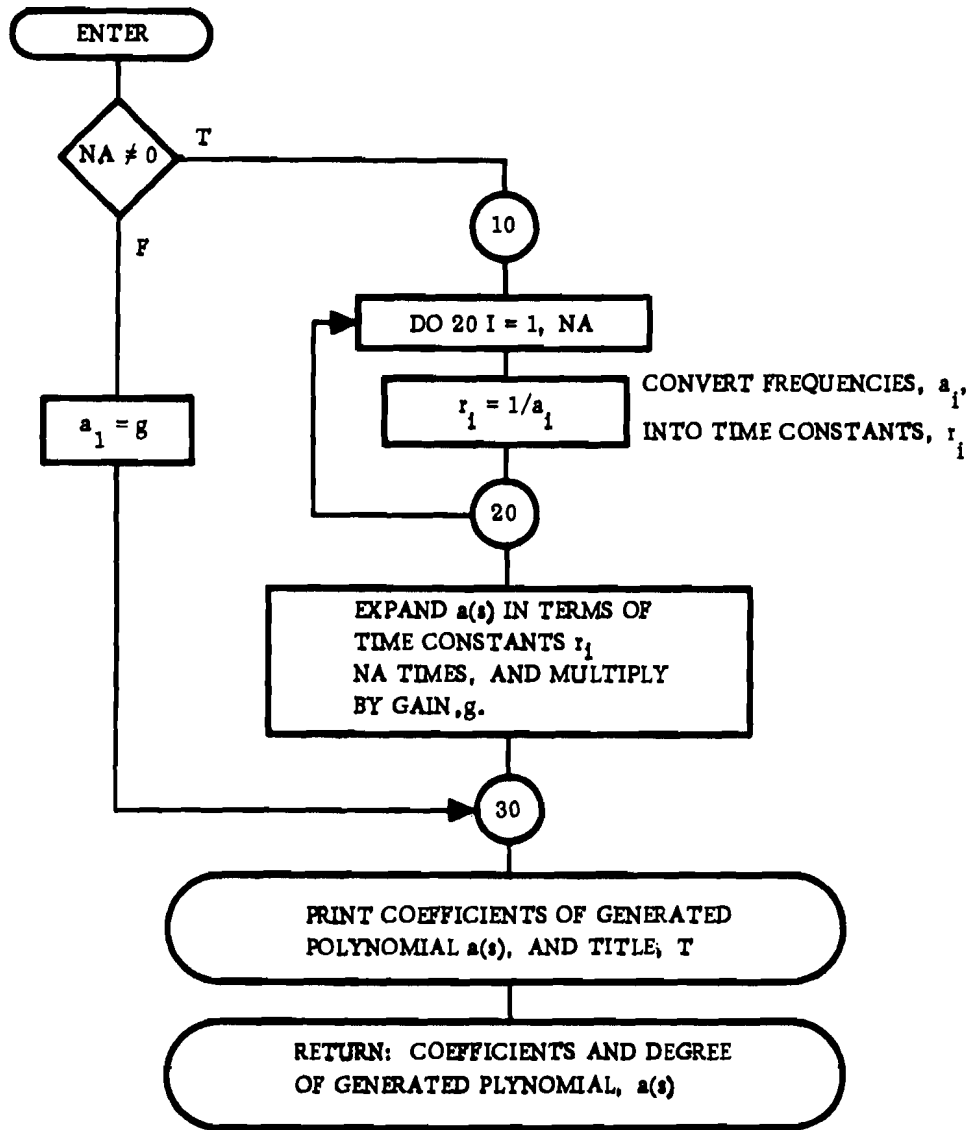


Figure 10. Flowchart for Subroutine GENP

Table XIII. Fortran H Program Listing for Subroutine GENP

	SUBROUTINE GENP(A,NA,G,T,NT)	X1000010
C	THIS SUBROUTINE GENERATES A POLYNOMIAL OF THE FORM	X1000020
C	$G*(1+S/A(1))(1+S/A(2))\dots(1+S/A(NA))$	X1000030
C		X1000040
	REAL*4 A(1),T(1),R(8)	X1000050
	IF(NA.LT.0)RETURN	X1000060
	IF(NA.NE.0)GO TO 10	X1000070
	A(1)=G	X1000080
	GO TO 30	X1000090
	10 DO 20 I=1,NA	X1000100
	20 R(I)=1./A(I)	X1000110
	A(I)=1.	X1000115
	CALL XPNTAU(R,NA,A,0,NA)	X1000120
	CALL GPOL(A,NA,G,A,NA)	X1000130
	30 CALL WRTPOL(A,NA,T,NT)	X1000140
	RETURN	X1000150
	END	X1000160

## V. CONCLUSION AND RECOMMENDATIONS

Computer programs TJET and TFAN have been valuable in the linear control analysis for the Propulsion System Flow Stability Program. The efficiency of these programs are such that many flight cases can be evaluated in a relatively short time to achieve the primary goal of designing rapid responding closed loop control systems.

The reasons that TJET and TFAN were developed rather than using an existing root locus computer program for the analysis are:

1. Some control loops (the turbojet rotor speed control, and turbofan high pressure rotor speed control loops) have more than one feedback, which requires more than one computer run on a general root locus computer program. TJET and TFAN combine all the necessary polynomial terms for the root locus analysis of these control loops automatically in one computer run.
2. Data handling is facilitated by (a) the conversion of transfer function data of the form supplied by P&WA in terms of the natural frequencies and steady-state gains into s-plane polynomial coefficients, (b) the actuator and sensor time constants for each control loop is combined automatically with the appropriate polynomial terms, and (c) all gains due to transfer function dynamics, actuator and sensor lags and initial operating point data are computed correctly, eliminating the time consuming process and reducing the probability of error in computing the correct gains by hand calculations.
3. Each control loop and control gain in the print-outs of TJET and TFAN are identified as such for easy reference.

It is recommended that the following modifications and additions to TJET and TFAN be made to increase the efficiency in designing and evaluating linear control systems for the turbojet and turbofan engines.

1. Include the capability of analyzing coupled engine control systems by adding the necessary cross-coupling terms in the polynomial equations to account for the interaction between control loops. The structures of TJET and TFAN are set up such that the cross-coupling numerators necessary for the analysis of coupled control loops can be easily included with minor modifications to TJET and TFAN.
2. Include the capability of analyzing the inlet duct control loops. This capability, when coupled to (1) above, should enable analysis of the complete system with cross-coupling (interaction).
3. To facilitate the transient analysis and the design of rapid responding control systems, an exponential least squares fit subprogram described in Part XIX, Appendix B should be included so that the effective closed loop step response time constants can be printed out along with the root locus.



4. If the cross-coupling transfer functions are included at a later date, then it should be possible to compute and minimize by decoupling gains the integral square error in one control loop due to a reference input into another loop.
5. To facilitate the root locus analysis, the outputs from TJET and TFAN can be modified to include
  - a. CRT (Cathode Ray Tube) plots of the root locus as an option, and
  - b. the print-outs of the damping ratios and natural frequencies of the computed complex pair closed loop poles of the root locus.

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5. AUTHOR(S) (First name, middle initial, last name) Evan L. Lum			
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13. ABSTRACT <p>This part describes computer programs developed to handle the computational tasks for the linear stability analysis of propulsion controls by root locus techniques. The descriptions, flowcharts, and Fortran program listings of two main programs TJET and TFAN developed for the analysis of turbojet and turbofan engine control systems are presented. Also presented are the descriptions of three subroutines specially developed to facilitate data handling for this study. Examples are given to illustrate the application of computer programs TJET and TFAN.</p> <p>TJET and TFAN have been valuable in the linear analysis of the propulsion system. However, it is recommended that these computer programs be expanded to include the capability of analyzing coupled control loops and to include a limited transient analysis.</p>			

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
Root Locus Turbojet Control Loop Analysis Turbofan Control Loop Analysis Computer Program for Gas Turbine Engine Control Analysis						

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